
Rotation profile modifications by RWMs and rotation control with RWM feedback

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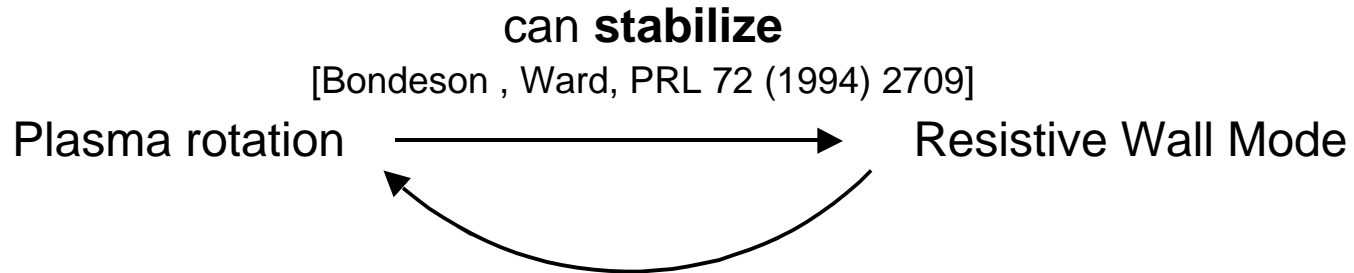
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University*

Motivation

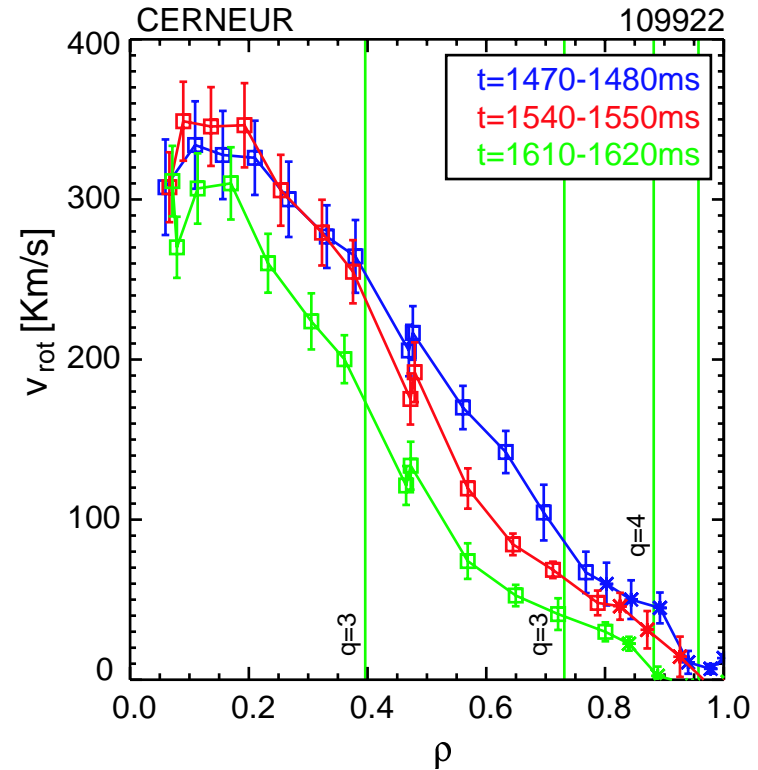
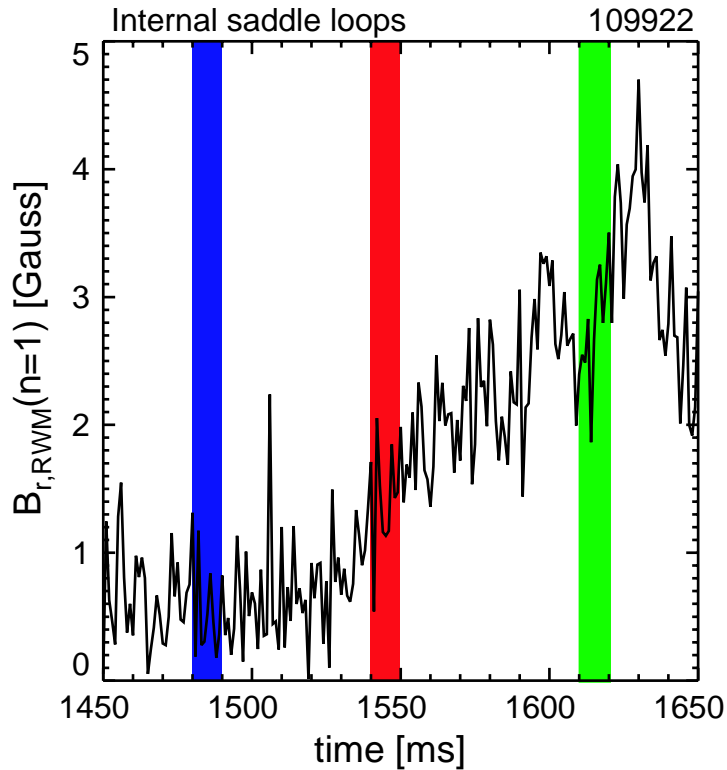


Finite amplitude RWM exerts drag

- Minimizing the drag essential for sustained rotational stabilization of the RWM. Key discovery: ‘Error field amplification’ [Boozer, PRL 86 (2001) 5059]
 - Effect of finite amplitude RWM on rotation profile.
 - Compare rotation decay with ‘transit time magnetic pumping’.
- Use additional drag to access a low-rotational regime for feedback control of the RWM without the stabilizing effect of plasma rotation.
 - Combine RWM braking with RWM feedback control.

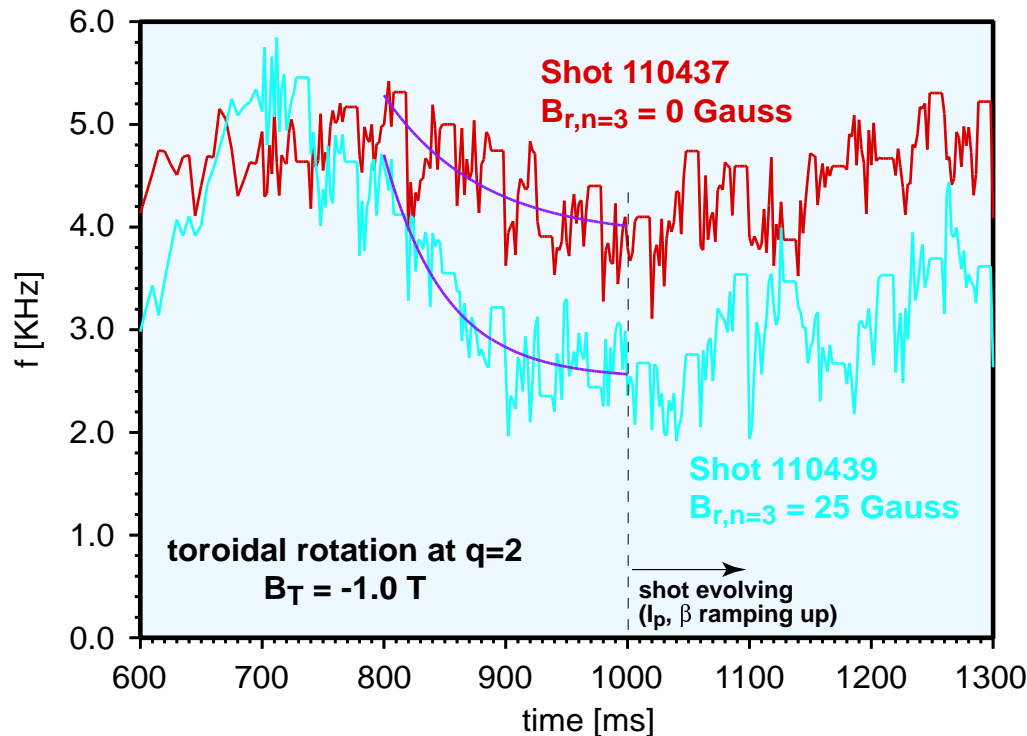
Finite amplitude RWM slows plasma across entire profile

- Use external $n=1$ field to excite marginally stable RWM (resonant field amplification - RFA).



Drag of external non-resonant field described by “Transit Time Magnetic Pumping”

Apply $m/n=1/3$ external field
(no resonant interaction with RWM)



[T. Scoville et al, APS, Orlando 2002]



Rotation decay for “transit time magnetic pumping”

$$\frac{df}{dt} = \frac{f_0 - f}{\tau_L} - C_{\text{ttmp}} \left(\frac{B_r}{B_T} \right)^2 f$$

Fit results:

$$f_0 = 3.9 \text{ KHz}$$

$$C_{\text{ttmp}} = 8.7 \cdot 10^5 \text{ s}^{-1}$$

Calculate C_{ttmp} from profiles
[La Haye et al, PP 9 (2002) 2051]:

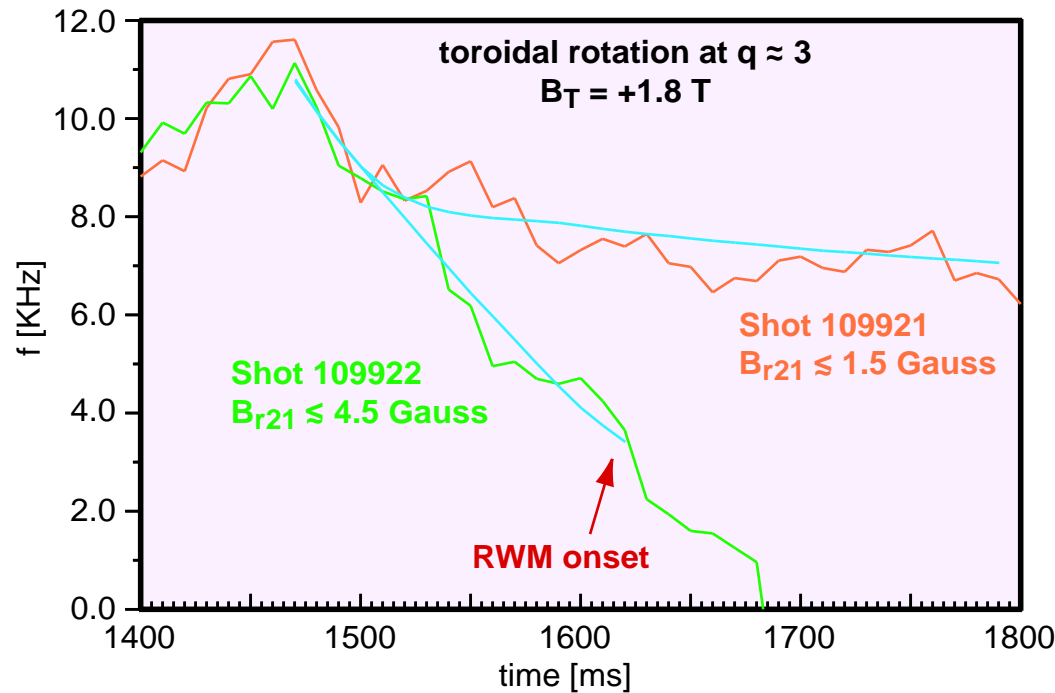
$$C_{\text{ttmp}} = 3.1 \cdot 10^5 \text{ s}^{-1}$$

Predicted value **just** three times smaller.

Drag of finite amplitude RWM too large to be explained by TTMP

Apply n=1 external field (resonant interaction with RWM, but no q=2 surface)

Rotation decay for “transit time magnetic pumping”



[T. Scoville et al, APS, Orlando 2002]

$$\frac{df}{dt} = \frac{f_0 - f}{\tau_L} - C_{\text{ttmp}} \left(\frac{B_r}{B_T} \right)^2 f$$

Fit results:

$$f_0 = 15.5 \text{ KHz}$$

$$C_{\text{ttmp}} = 1.0 \cdot 10^9 \text{ s}^{-1}$$

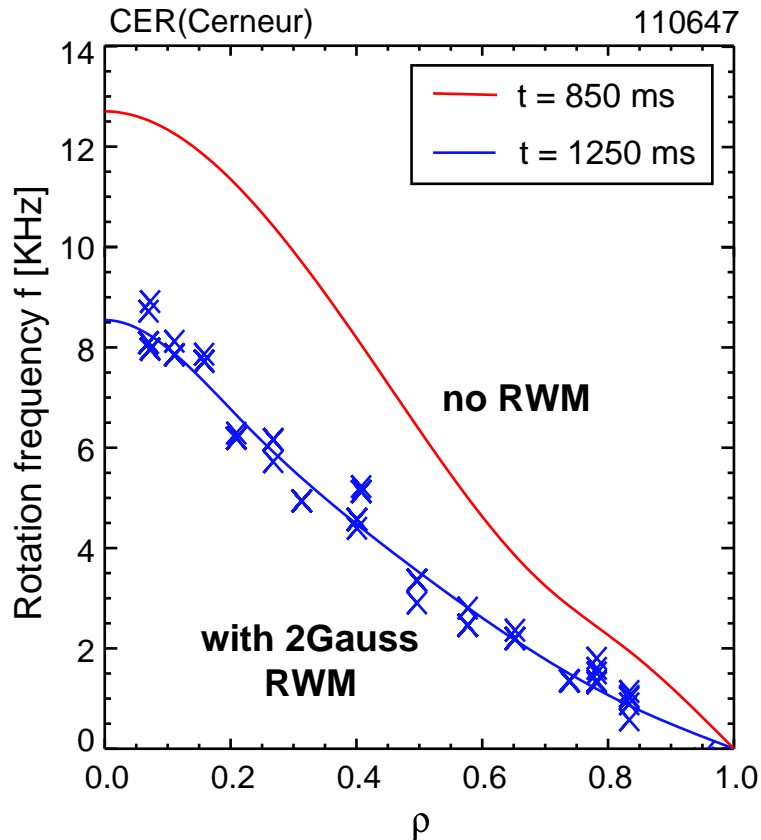
Calculate C_{ttmp} from profiles [La Haye et al, PP 9 (2002) 2051]:

$$C_{\text{ttmp}} = 5.1 \cdot 10^5 \text{ s}^{-1}$$

The braking field has to be at least 25 times larger than the applied external field. Observed is an order of 1.



Can we use a finite amplitude RWM to access a low rotational regime for direct feedback control?



RWM ($B_r(\text{wall})=2$ Gauss) in a 1T plasma:

- Uniform braking.
 - Reduction of momentum confinement τ_L by 70%.
 - Reduction of energy confinement τ_E by 30%.
- **RWM is an efficient brake.**

Idea: Combine n=1 braking with RWM feedback.

→ Control the RWM at a finite amplitude (rather than 0).

Feedback control on a finite amplitude RWM

Apply C-coil field B_{ext} , if detected error B_{err} is not equal to a requested B_{offset} .

$$B_{\text{ext}} = -PID(B_{\text{err}} - B_{\text{offset}})$$

PCS (choose proportional gain G_P and a pre-programmed C-coil offset I_{offset} , neglect derivative and integral gain):

$$B_{\text{ext}} = M_C I_{\text{offset}} - G_P B_{\text{err}}$$

Plasma response described by resonant field amplification of a marginally stable RWM (phenomenological):

$$B_{\text{RWM}} = A_{\text{RFA}} B_{\text{ext}}$$

Using “mode-control” ($B_{\text{err}} = B_{\text{RWM}}$) the resulting equilibrium RWM amplitude is:

$$B_{\text{RWM}} = \frac{A_{\text{RFA}}}{1 + A_{\text{RFA}} G_P} \cdot M_C I_{\text{offset}}^*$$



* I_{offset} defined with respect to the optimum correction currents of the intrinsic error field.

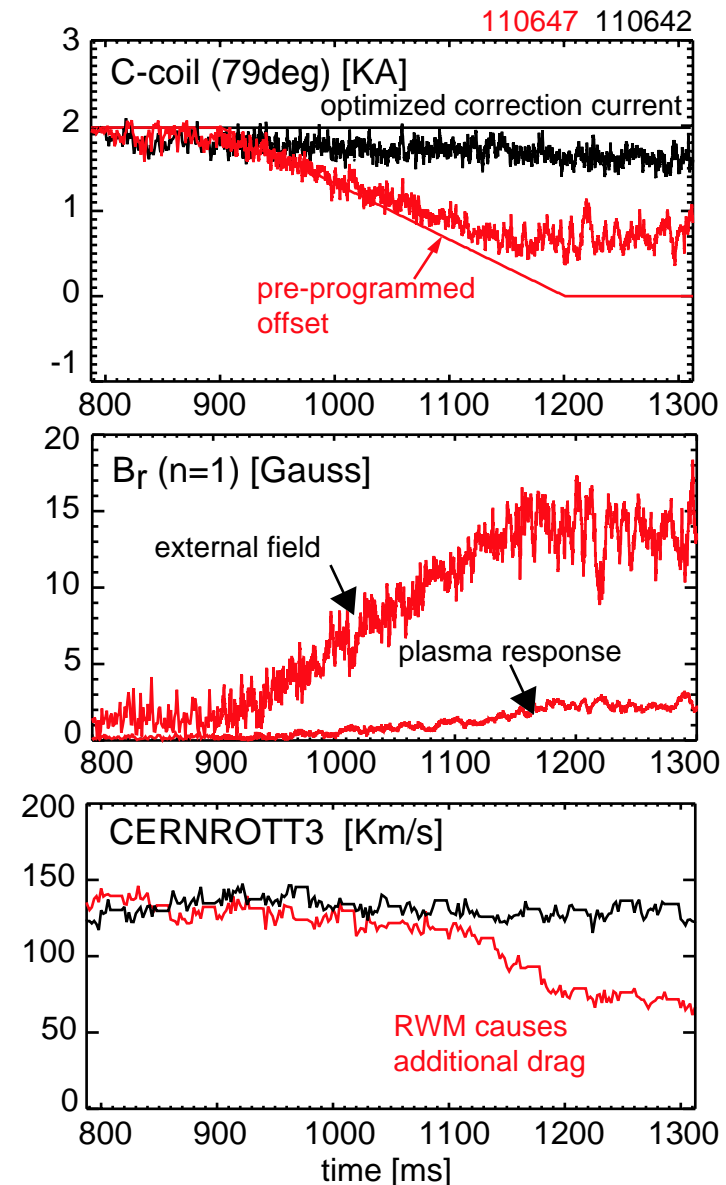
Feedback with a pre-programmed current offset excites marginally stable RWM

In the presence of RFA the feedback system will partially compensate I_{offset} ,

$$I_C = \frac{1}{1 + A_{\text{RFA}} G_P} \cdot I_{\text{offset}}$$

Experiment: Apply a pre-programmed offset to the optimum C-coil currents at $\beta > \beta_{\text{no-wall}}$:

- Partial correction of the C-coil offset corresponds to $A_{\text{RFA}} \sim 0.15$.
- Consistent with an observed $A_{\text{RFA}} \sim 0.17$ measured by magnetic probes.



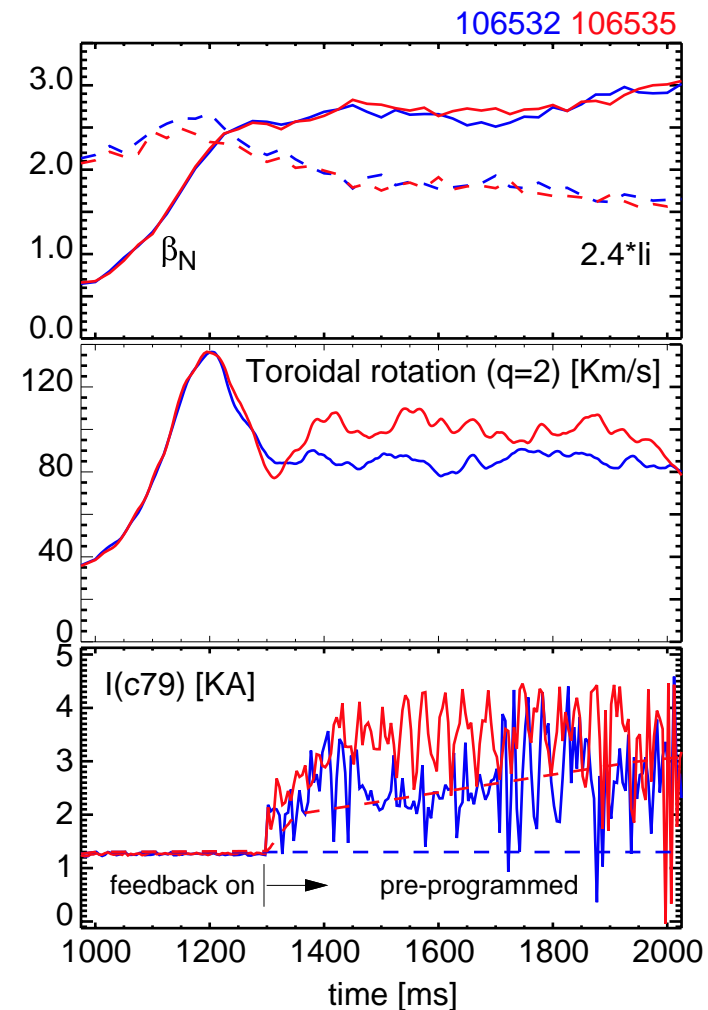
RWM feedback finds optimum correction current

Optimize C-coil currents to minimize the RFA amplitude and, hence, drag.

- Feedback reduces the difference between pre-programmed and optimum correction currents,

$$I_C = \frac{1}{1 + A_{RFA} G_P} \cdot I_{offset}$$

- The improvement is typically ~50% ($G_P \sim 5$, $A_{RFA} \sim 0.2$)
- Several iterations improve the correction currents.



[Garofalo et al, NF 42 (2002) 1335]

Extension of feedback model to an unstable RWM shows that an applied offset does not change the condition for stability

Assume,

$$\delta W_{\text{RWM}} \propto B_{\text{RWM}}^2$$

and

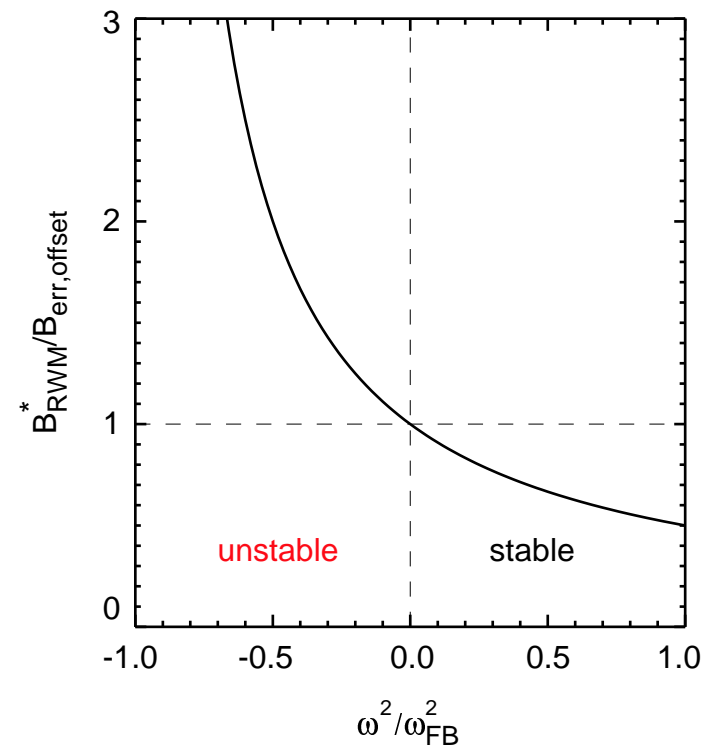
$$F_{\text{ext}} \propto B_{\text{ext}}$$

Then, the condition for stability,

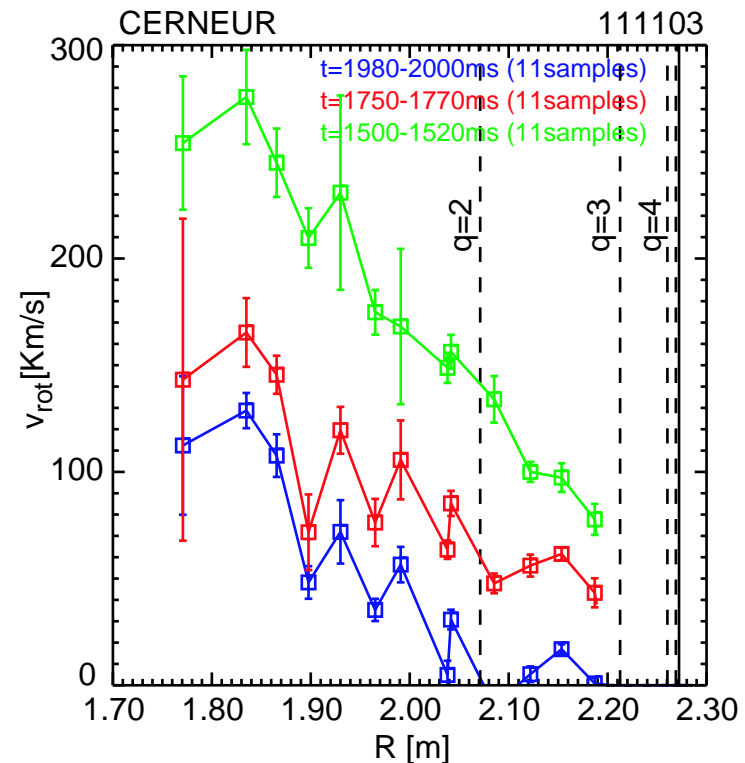
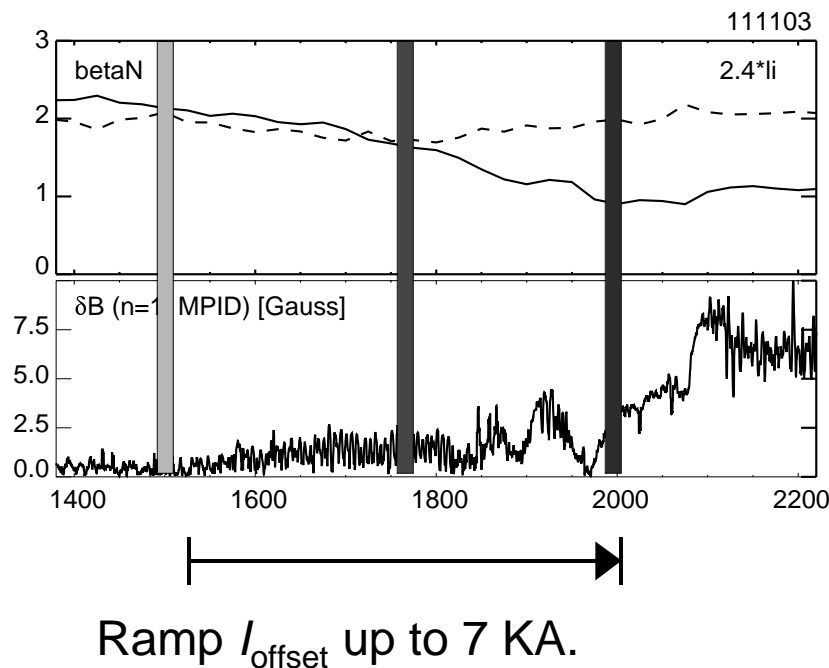
$$\omega^{*2} = \omega^2 + \frac{G_P \alpha}{K} > 0$$

is independent of the offset.

B_{RWM} , however, increases continuously with decreasing RWM stability \rightarrow **non-linear** effects more likely to become important.



RWM braking at low rotation can generate magnetic islands



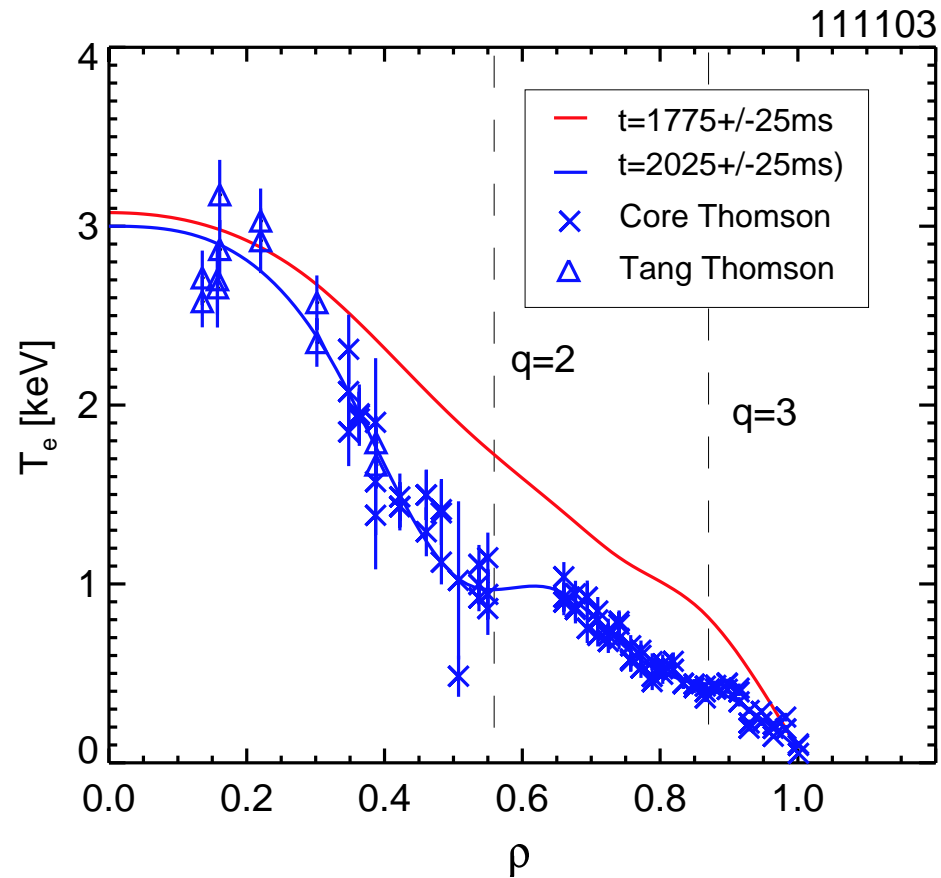
- RFA of marginally stable RWM → **global braking**.
- Large external n=1 field at low rotation creates magnetic islands → local braking and bad confinement.



Avoid large external field at low rotation with a rotation dependent $I_{C,\text{offset}}$

External field at low rotation causes magnetic islands

- RWM braking $\rightarrow T_e$ profile shows no islands.
- Large external $n=1$ field at low rotation $\rightarrow T_e$ profile shows signature of 2/1 and 3/1 islands.



Summary

Effect of RWM on rotation profile

- The RWM causes a rotation decay across the entire profile.
- The RWM drag is too large to be explained by 'transit time magnetic pumping' alone.

Combine RWM braking with RWM feedback

- Pre-program C-coil current offset is only partially corrected by RWM feedback and excites marginal stable RWM for additional drag.
- RWM feedback can iteratively improve correction of intrinsic error field.
- RWM braking at low rotation prone to island generation → need to maintain rotation above a critical value.

