

# **Extended Lumped Parameter Model of Resistive Wall Mode and The Effective Self-Inductance**

**M.Okabayashi, M. Chance, M. Chu\* and R. Hatcher  
A. Garofalo\*\*, R. La Haye\*, H. Remeirdes\*\*, T. Scoville\*, and T. Strait\***

**Princeton Plasma Physics Laboratory**

**\* General Atomics**

**\*\* Columbia Univeristy**

**"Active Control of MHD Stability: Extension of Performance" Workshop  
under the auspices of the US/Japan Collaboration  
at Columbia University, 18 -20 November 2002**

# OUTLINE

## - Extended Lumped Parameter Model and RWM Effective Self-Inductance

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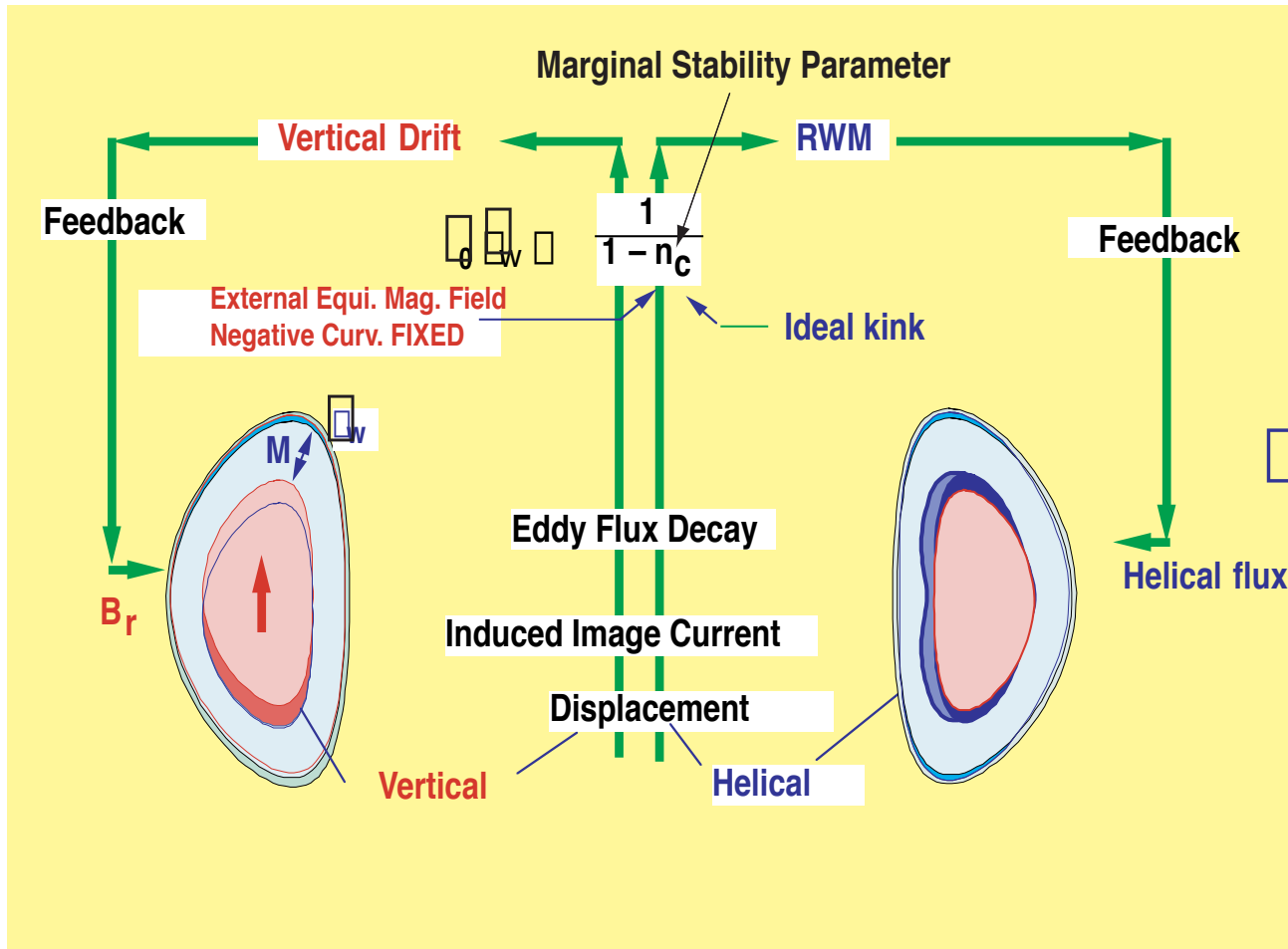
- MOTIVATION
- APPROACH AND ASSUMPTIONS OF EXTENDED LUMPED PARAMETER MODEL
  - Relation to recent other approaches (models)
- "RWM EFFECTIVE SELF-INDUCTANCE"
  - Plasma response is conveniently characterized by one parameter
- APPLICATIONS
  - Dispersion relation / Initial value time dependent solution
  - Resonant magnetic braking,
  - Non-resonant braking,
  - Resonant Field Amplification

# MOTIVATION

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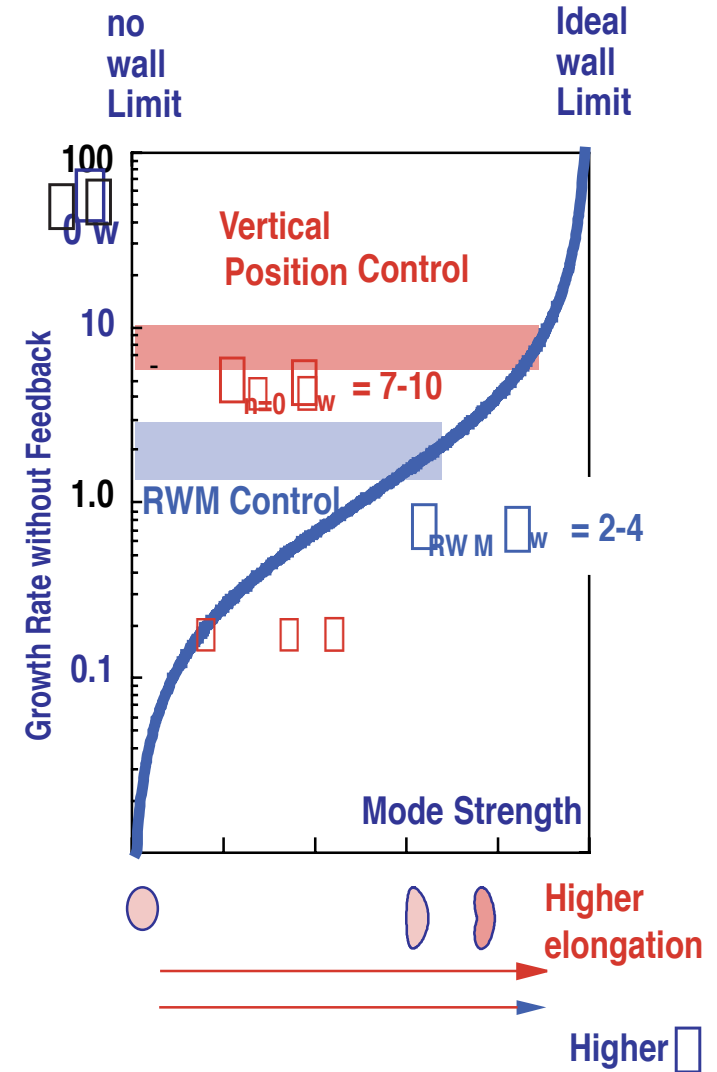
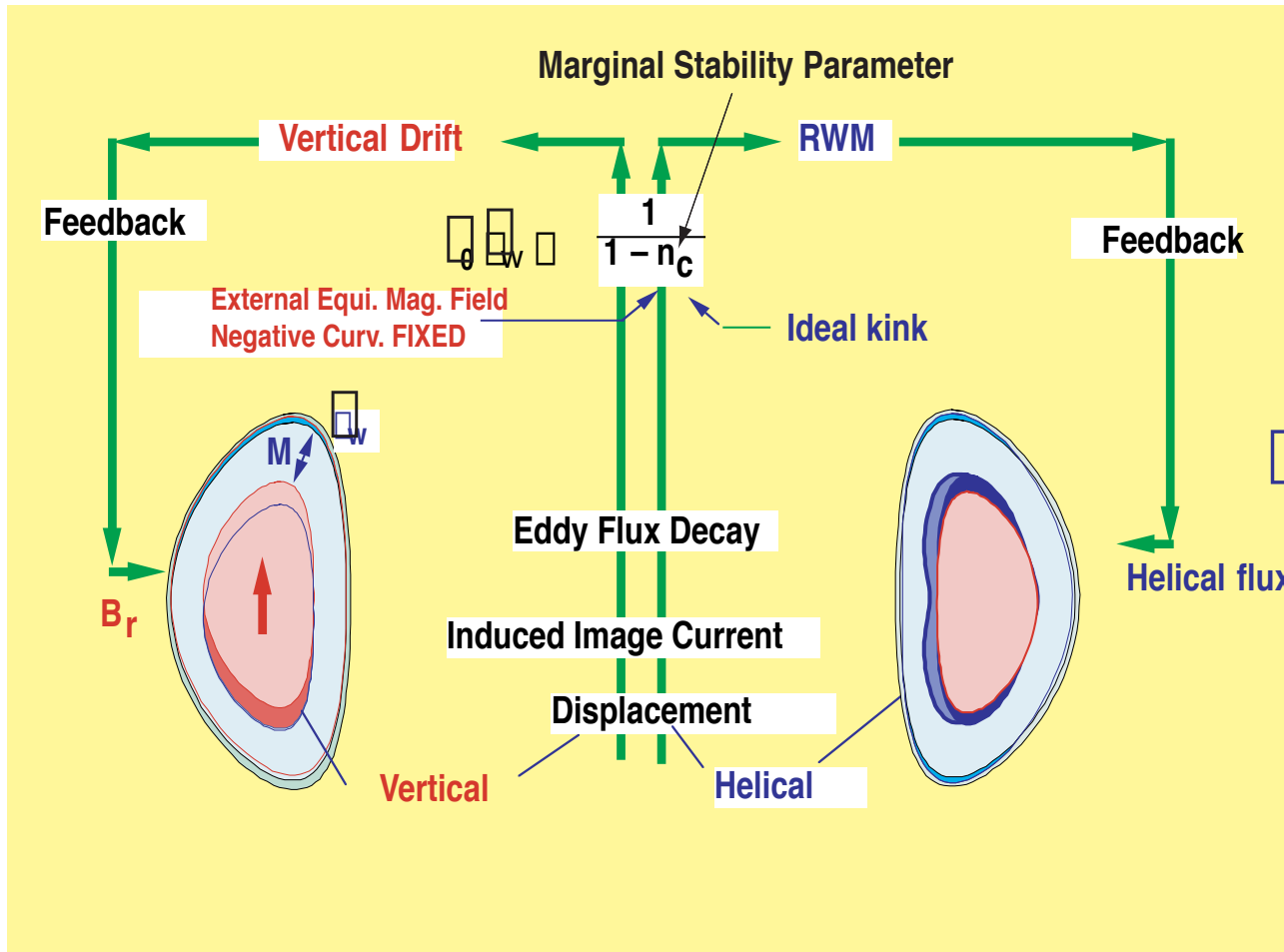
- Develop simple description of RWM stabilization process, useful for qualitative and semi-quantitative discussion.
  - M. Okabayashi, N. Pomphrey and R. Hatcher, N. Fusion. 38(1998) 1607
  - M. Okabayashi et al, EPS 2002 (Plasma Phy. and Controlled Fusion in press)
  
- The model to be consistent with MHD analysis models developed by various groups
  - A. Bondeson and D. Ward, Phys. Rev. Lett. 72 (1994)2709
  - J. Bialek, et al., Phys. of Plasmas, 8 (2001) 2170
  - M. Chu et al., (IAEA 2002)
  - R. Fitzpatrick, Phy. Plasmas 9 (2002) 3459
  - A. Garofalo, Sherwood meeting (2002)

# RWM AND ITS FEEDBACK CONTROL CAN BE CONSIDERED AS THE $n=1$ HELICAL INSTABILITY ANALOG TO THE $n=0$ VERTICAL INSTABILITY



- "Mode Rigidity" is the fundamental assumption

# RWM AND ITS FEEDBACK CONTROL CAN BE CONSIDERED AS THE $n=1$ HELICAL INSTABILITY ANALOG TO THE $n=0$ VERTICAL INSTABILITY



- "Mode Rigidity" is the fundamental assumption

# Approach and Assumptions of Extended Lumped Parameter Model

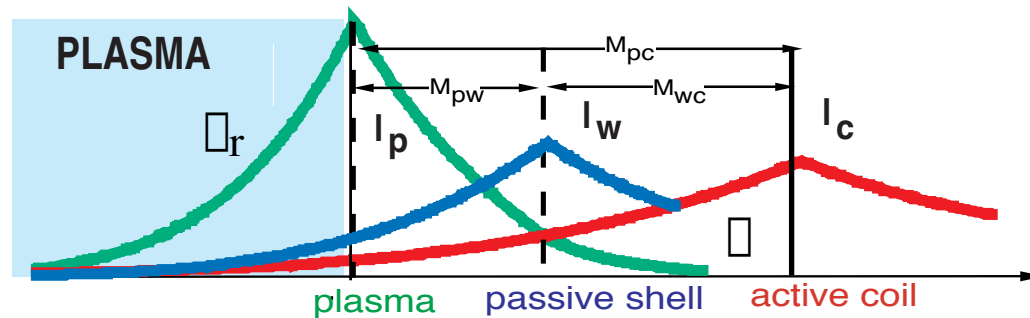
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- Include essential RWM physics
  - Pressure balance and B-normal continuity on plasma surface
  - Rotation dissipation in adhoc manner, however, consistent with existing theories
- Assumptions
  - Rigid displacement:  
justifiable based on experiments [M. Okabayashi et al., Phys. Plasmas 8,2071(2001)]
  - Cylindrical geometry
  - One mode excitation
  - No coupling to other [stable] modes

# EXTENDED LUMPED PARAMETER RWM MODEL

- **Explicit Usage of Boundary Conditions**

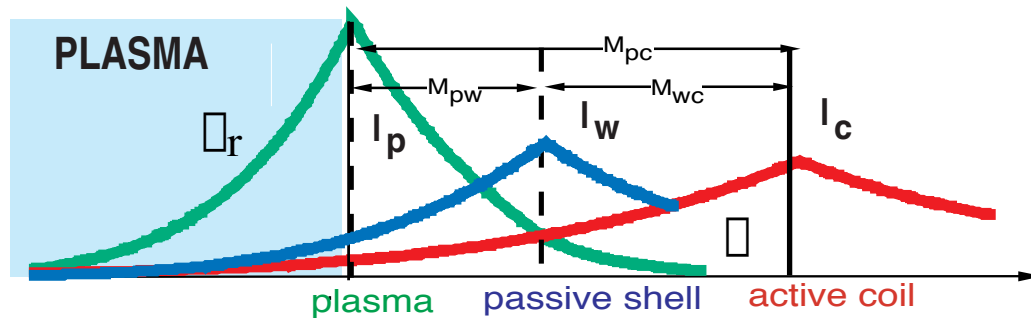
- on the Plasma Surface, Wall and Coil ( $I_p$ ,  $I_w$ ,  $I_c$ )
- Independent parameters: plasma skin current, wall current, feedback coil current



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## • Explicit Usage of Boundary Conditions

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- Independent parameters: plasma skin current, wall current, feedback coil current



## • Pressure Balance and B-normal Continuity on Plasma Surface

plasma displacement  $\frac{1}{r} \frac{d(r\delta_r)}{dr} \Big|_{r=a}$     rotational dissipation  $\delta_r (\delta_r + \delta_\theta \delta_\theta)$     plasma rotation  $m - nq$     external displacement  $\delta = \sum_i \sum_j \delta_{ij}$

$$\frac{1}{r} \frac{d(r\delta_r)}{dr} \Big|_{r=a} + \delta_r (\delta_r + \delta_\theta \delta_\theta) = (mf^2 / \mu_A^2 + f^2) (a \delta_r'(a_+) / m \delta_r(a_+) + 2 / f)$$

fixed displacement  $\delta_0$   
approximation

(available from experiment)

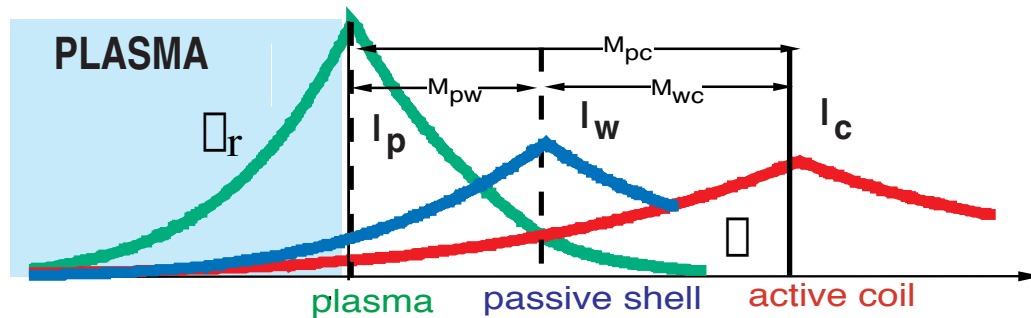
toroidal number



# EXTENDED LUMPED PARAMETER RWM MODEL

## • Explicit Usage of Boundary Conditions

- on the Plasma Surface, Wall and Coil ( $I_p, I_w, I_c$ )
- Independent parameters: plasma skin current, wall current, feedback coil current



## • Pressure Balance and B-normal Continuity on Plasma Surface

$$\left. \frac{1}{r} \frac{d(r\alpha)}{dr} \right|_{r=a} + \alpha (\alpha + \frac{m-nq}{r}) = (mf^2 / \alpha_A^2 + f^2) (\alpha'(a_+) / m\alpha(a_+) + 2/f)$$

plasma displacement  $\alpha$ , rotational dissipation  $\alpha$ , plasma rotation  $\alpha$ , external displacement  $\alpha = \sum_i \alpha_i \alpha_j$ , standard mutual inductance.

fixed displacement approximation  $\alpha_0$ , toroidal number  $m-nq$ .

## • Conveniently formulated "RWM effective self-inductance"

$$V = d/dt \begin{pmatrix} L_{eff} & M_{pw} & M_{pc} \\ M_{wp} & L_w & M_{wc} \\ M_{pc} & M_{cw} & L_c \end{pmatrix} \begin{pmatrix} I_p \\ I_w \\ I_c \end{pmatrix}$$

$$L_{eff} I_p + M_{pw} I_w + M_{pc} I_c = 0$$

$$L_{eff} = \left( \alpha_0 \alpha_n + \alpha(\alpha + \frac{m-nq}{r}) \right) L / \left( \alpha_0 \alpha_n^{-2} + \alpha(\alpha + \frac{m-nq}{r}) \right)$$

$$\alpha_n = 2/f - 1 \quad (f=1 \leftrightarrow \text{no wall limit}, \alpha_n=1)$$

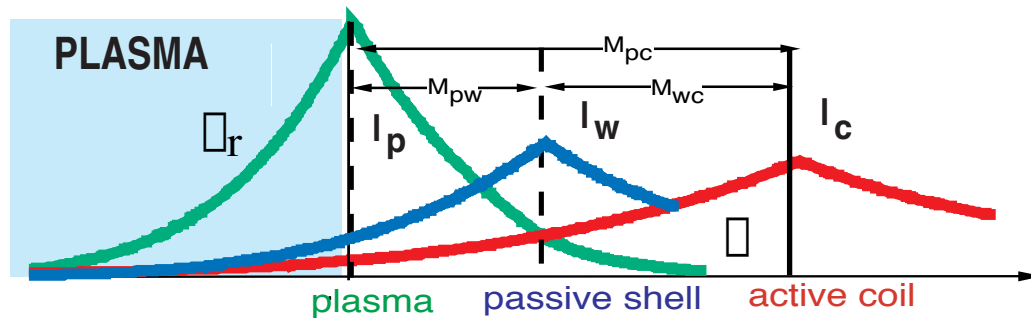
standard mutual inductance

•  $L_{eff}$  represents all RWM characteristics currently considered

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- on the Plasma Surface, Wall and Coil ( $I_p, I_w, I_c$ )
- Independent parameters: plasma skin current, wall current, feedback coil current



## • Pressure Balance and B-normal Continuity on Plasma Surface

$$\left( \frac{1}{\mu_0} \frac{d(r\mu_0)}{dr} \right)_{r=a} + \mu_0 (\mu + \mu_0 \mu_0) = (m - nq)^2 \frac{mf^2}{\mu_0^2 \mu_A^2 + f^2} \left( a \mu_0'(a_+) / m \mu_0(a_+) + 2/f \right)$$

fixed displacement approximation  $\mu_0$

toroidal number

magnetic decay index  $N''z + Br_{ext} = 0$  : vertical instability

## • Conveniently formulated "RWM effective self-inductance"

$$V = d/dt \begin{pmatrix} L_{eff} & M_{pw} & M_{cp} \\ M_{wp} & L_w & M_{wc} \\ M_{pc} & M_{cw} & L_c \end{pmatrix} \begin{pmatrix} I_p \\ I_w \\ I_c \end{pmatrix}$$

$$L_{eff} I_p + M_{pw} I_w + M_{pc} I_c = 0$$

$$L_{eff} = \frac{(\mu_0 \mu_0 \mu_n + \mu(\mu + \mu_0 \mu_0)) L}{(\mu_0 \mu_0 \mu_n^{-2} + \mu(\mu + \mu_0 \mu_0))}$$

standard mutual inductance

$$\mu_n = 2/f - 1 \quad (f=1 \leftrightarrow \text{no wall limit, } \mu_n=1)$$

$L_{eff}$  represents all RWM characteristics currently considered

# RWM Dispersion Relation

- Dispersion Relation with Extended Lumped Parameter Model Expresses Explicitly Geometrical Elements

- Extended Lumped Parameter Model

$$\begin{array}{c}
 \text{kinetic} \\
 | \\
 [ c_k (\omega + i\nu)^2 + \nu(\omega + i\nu) + \nu_0 - \nu_n ] (\omega + \nu_w^{-1}) - \nu [ c_k (\omega + i\nu)^2 + \nu(\omega + i\nu) + \nu_0 - \nu_n - 2 ] (M_{pw}^2 / L_w L_p ) = 0
 \end{array}$$

dissipation
plasma beta
wall time constant
geometrical term
 $M_{ij} = (r_i/r_j)^m$

# RWM Dispersion Relation

- Dispersion Relation with Extended Lumped Parameter Model Expresses Explicitly Geometrical Elements

- Extended Lumped Parameter Model

$$\begin{aligned}
 & \text{kinetic} \quad \text{dissipation} \quad \text{plasma beta} \quad \text{wall time constant} \quad \text{geometrical term} \quad M_{ij} = (r_i/r_j)^m \\
 & [c_k(\omega + i\nu)^2 + \nu(\omega + i\nu) + \beta_0 - \beta_n](\omega + \omega_w^{-1}) - [c_k(\omega + i\nu)^2 + \nu(\omega + i\nu) + \beta_0 - \beta_n - 2] (M_{pw}^2 / L_w L_p) = 0
 \end{aligned}$$

- Fitzpatrick's "Simple Model of RWM..." in Phys. Plasmas 9(2002)3459

## E. RWM dispersion relation

Neglecting the error field, for the moment, Eqs. (5), (8), (9), and (10) can be combined to give the following simple cubic RWM dispersion relation:

$$\begin{aligned}
 & \text{kinetic} \quad \text{plasma beta} \\
 & [(\hat{\gamma} - i\hat{\Omega}_\phi)^2 + \nu_*(\hat{\gamma} - i\hat{\Omega}_\phi) + (1 - \kappa)(1 - md)] \\
 & \text{dissipation*} \quad \times (\hat{\gamma}S_* + 1 + md) = 1 - (md)^2. \quad \text{geometrical term} \quad (12) \\
 & \text{wall time constant*}
 \end{aligned}$$

$$d = \frac{1}{m} \frac{(r_w/a)^{2m-1}}{(r_w/a)^{2m+1}},$$

$$d_c = \frac{1}{m} \frac{(r_c/a)^{2m-1}}{(r_c/a)^{2m+1}},$$

## GENERAL FORMULATION INCLUDING PLASMA ROTATION AND DISSIPATION

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- The resistive wall mode can be described in terms of circuits on the resistive wall driven by the plasma or the external coils

$$\frac{\mu_0 \Delta z}{\eta \lambda_{l'_w}} \frac{\partial B_{l'_w}}{\partial t} + \sum_{l_w} M_{l'_w l_w} B_{l_w}^w = \sum_{l_p} C_{l'_w l_p}^{wp} B_{l_p}^p - \sum_{l_c} C_{l'_w l_c}^{wc} I_{l_c} \quad (7)$$

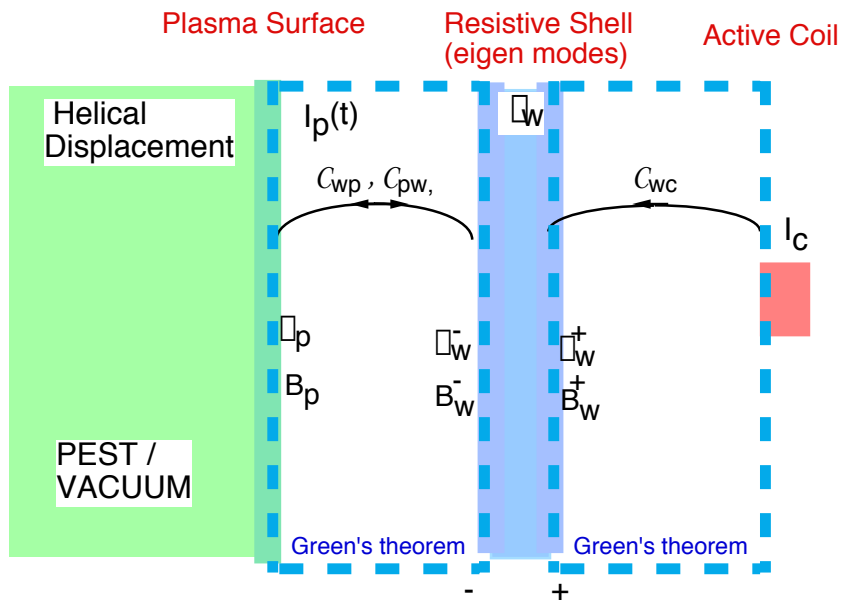
- The plasma responds to the magnetic field  $B_{l_w}$  on the resistive wall through the relationship

$$B_{l_p}^p = - \frac{1}{\delta W_{I_w} + i \Omega D} C_{l_p l_w}^{pw} B_{l_w}^w \quad (8)$$

- The response of the RWM to the coil currents is therefore

$$\frac{\mu_0 \Delta z}{\eta \lambda_{l'_w}} \frac{\partial B_{l'_w}}{\partial t} + \sum_{l_w} \left( M_{l'_w l_w} + \sum_{l_p} C_{l'_w l_p}^{wp} \sum_{l'_p} \frac{1}{(\delta W_{I_w} + i D \Omega)_{l_p l'_p}} C_{l'_p l_w}^{pw} \right) B_{l_w}^w = - \sum_{l_c} C_{l'_w l_c}^{wc} I_{l_c} \quad (9)$$

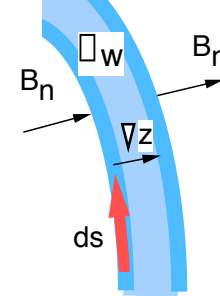
# Schematics of RWM Feedback Analysis with Toroidal Geometry



## Resistive Wall Thin Shell Approximation

- Introducing "skin current stream function"  $\psi_w$ :  $j = \nabla z \times \nabla \psi_w(z-z_w)$
- normal magnetic field continuity  $\psi / \eta^{(-)} = \psi / \eta^{(+)} = B_n$
- Ampere's Law:  $\psi(+)-\psi(-) = \psi_w$
- Faraday's Law

$$\nabla_s [\nabla_s \psi_w] = (\partial / \partial t) (B_n), \text{ assuming } |\nabla z| = 1$$



$\psi_w(\mathbf{r}, t)$  can be expanded in eigenmodes

Resistive Shell

## THE LUMPED PARAMETER MODEL AND RFA

- For the least stable resistive wall mode and assuming the matrix elements of the energy and dissipation factors are constants, we arrive at a "lumped parameter equation"

$$\tau_w \frac{\partial B_w}{\partial t} + M \frac{1}{A} B_w = C^{wc} I_c \quad (10)$$

the total RWM field at wall  
external helical current

where A is the 'complex amplification factor'. Note that A = 1 in the absence of plasma

$$A = \frac{\square W_{/W}(\square) + \square \square \square}{\square W_{nW}(\square) + \square \square \square} \quad (11)$$

potential energy with ideal wall  
potential energy without wall

- In this equation we see that the dissipation on the wall and the dissipation in the plasma are separated

1. 'No External Coil': homogeneous equation, dissipation in plasma and the resistive wall

$$\gamma \tau_w = -M \frac{1}{A} \quad (12)$$

2. 'Steady State with External Coil': inhomogeneous equation. dissipation in plasma

$$B_w = \frac{A}{M} C^{wc} I_c \quad (13)$$

# 1D FORMULATION AND LUMPED PARAMETER MODEL

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M. Chu Formulation (IAEA 2002)

Extended Lumped Parameter Model

- **growth rate**

total B-field on wall

$$\tau_w \frac{\partial B_w}{\partial t} + M \frac{1}{A} B_w = C^{wc} I_c$$

$$1/A = \frac{\partial W_{nw}(\omega) + \partial \dots}{\partial W_{iw}(\omega) + \partial \dots}$$

$$\gamma \tau_w = -M \frac{1}{A}$$

- **resonant field amplification**

$$B_w = \frac{A}{M} C^{wc} I_c$$



# W FORMULATION AND LUMPED PARAMETER MODEL

## M. Chu Formulation (IAEA 2002)

### • growth rate

total B-field on wall

$$\tau_w \frac{\partial B_w}{\partial t} + M \frac{1}{A} B_w = C^{wc} I_c$$

$$1/A = \frac{W_{nw}(\omega) + \dots}{W_{iw}(\omega) + \dots}$$

$$\gamma \tau_w = -M \frac{1}{A}$$

### • resonant field amplification

$$B_w = \frac{A}{M} C^{wc} I_c$$

## Extended Lumped Parameter Model

$$L_w \frac{\partial I_p}{\partial t} + [-L_{\text{eff}} / (L_{\text{eff}} - M_{pw}^2 / L_w)] I_p = 0$$

$$L_{\text{eff}} = (L_0 - L_n + \dots) / (L_0 - L_n^2 + \dots)$$

# W FORMULATION AND LUMPED PARAMETER MODEL

## M. Chu Formulation (IAEA 2002)

### • growth rate

total B-field on wall

$$\tau_w \frac{\partial B_w}{\partial t} + M \frac{1}{A} B_w = C^{wc} I_c$$

$$1/A = \frac{W_{nw}(\gamma) + \gamma}{W_{iw}(\gamma) + \gamma}$$

$$\gamma \tau_w = -M \frac{1}{A}$$

### • resonant field amplification

$$B_w = \frac{A}{M} C^{wc} I_c$$

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$$\frac{\partial I_p}{\partial t} + [-L_{\text{eff}} / (L_{\text{eff}} - M_{pw}^2 / L_w)] I_p = 0$$

$$L_{\text{eff}} = (\gamma_0 - \gamma_n + \gamma) \mu_0 / (\gamma_0 - \gamma_n^2 + \gamma)$$

- marginal stability  $\gamma$  (no wall limit)

$$\gamma_w = 0 \longleftrightarrow L_{\text{eff}} = 0 : \gamma_0 = \gamma_{n.w}$$

- Ideal wall limit

$$\gamma_w = \text{infinity} \rightarrow (L_{\text{eff}}(\gamma_{l.w}) - M_{pw}^2 / L_w) = 0$$

$$\gamma_w = \frac{(\gamma_{n.w} - \gamma_n + \gamma)}{(\gamma_{l.w} - \gamma_n + \gamma)} (\gamma_{n.w} - \gamma_{l.w}^2) / (\gamma^2)$$

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total B-field on wall

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$$1/A = \frac{W_{nw}(\gamma) + \gamma \gamma}{W_{iw}(\gamma) + \gamma \gamma}$$

$$\gamma \tau_w = -M \frac{1}{A}$$

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$$B_w = \frac{A}{M} C^{wc} I_c$$

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$$\gamma_w = \frac{(\gamma_{n.w} - \gamma_n + \gamma)}{(\gamma_{l.w} - \gamma_n + \gamma)}$$

$$(\gamma_{n.w} - \gamma_{l.w}^2) / (\gamma^2)$$

normalization constant

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total B-field on wall

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$$B_w = \frac{A}{M} C^{wc} I_c$$

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$$\mu_w = \frac{(\mu_{n.w} - \mu) + \mu \mu_n}{(\mu_{l.w} - \mu) + \mu \mu_n} \left( \frac{\mu_{n.w} - \mu \mu_n^2}{\mu^2} \right)$$

normalization constant

$$L_{\text{eff}} I_p + M_{pw} I_w + M_{pc} I_c = 0$$

$$I_p = \frac{M_{pc}}{L_{\text{eff}}} I_c$$

# RWM Time Evolution with Extended Lumped Parameter Model Plus Angular Momentum Balance

- Example(1): Magnetic Braking (Rotation slowing down with increasing mode amplitude)

$$\frac{\partial \theta}{\partial t} = \left( \frac{\theta_0}{m} \right) C_{vis} \operatorname{Im} [ I_p(t) I_c^*(t) ]$$

Steady target RWM amplitude coil current or error field  
 momentum conf. time ~1/ω ( R + iL ) -> 1/(iωL)  
 known as rotation dissipation "induction motor model"

# RWM Time Evolution with Extended Lumped Parameter Model Plus Angular Momentum Balance

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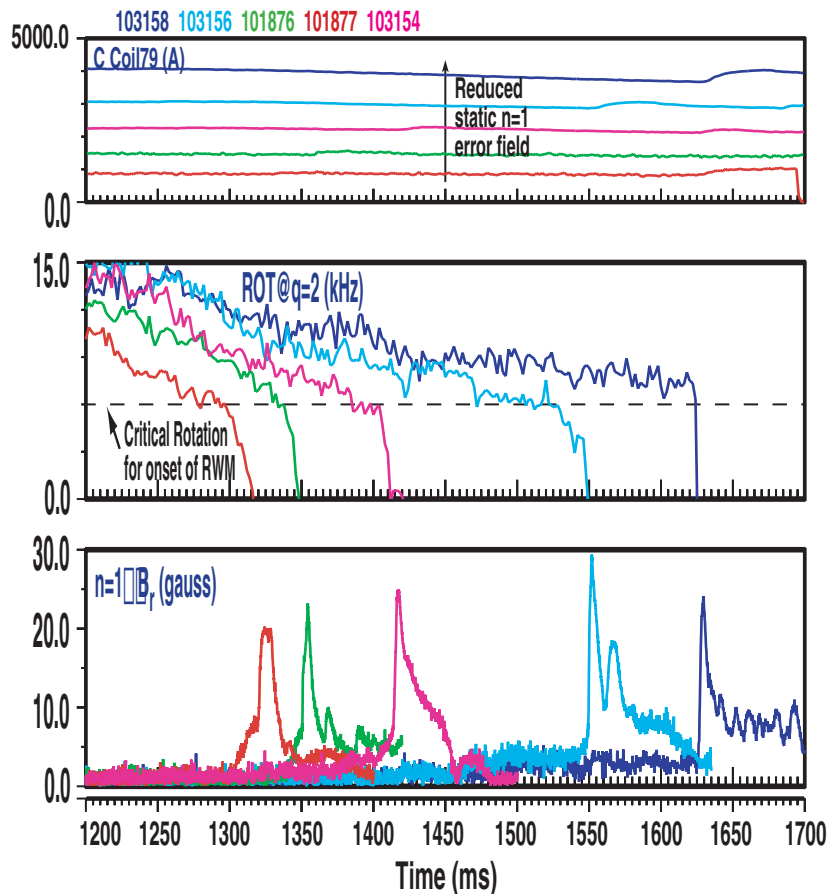
$$\frac{\partial \Omega}{\partial t} = (\Omega_0 \Omega) / \tau_m C_{vis} \text{Im}[\Omega_p(t) \Omega_c(t)]$$

Steady target RWM amplitude coil current or error field

momentum conf. time  $\sim 1/\Omega (\Omega + i\gamma) \rightarrow 1/(i\Omega\gamma)$

known as rotation dissipation "induction motor model"

## Experiment with Various External Fields



# RWM Time Evolution with Extended Lumped Parameter Model Plus Angular Momentum Balance

- Example(1): Magnetic Braking (Rotation slowing down with increasing mode amplitude)

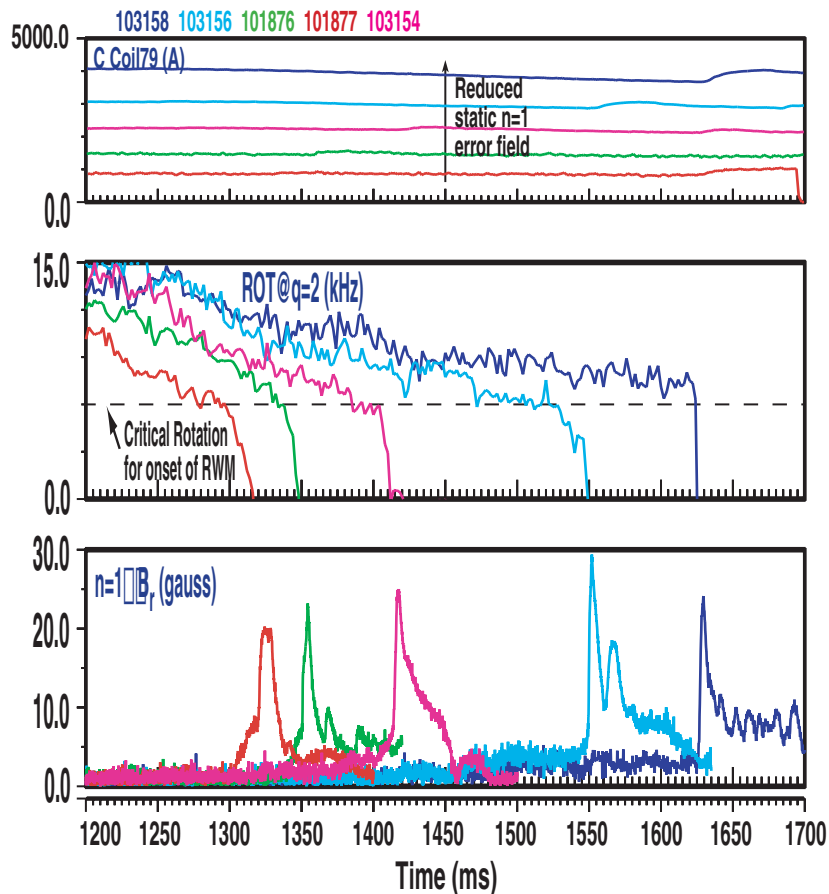
$$\frac{\partial \Omega}{\partial t} = \left( \frac{1}{\tau_0} - \frac{C_{vis}}{m} \text{Im} \left[ \frac{I_p(t)}{I_c} \frac{p(t)}{c} \right] \right) \Omega$$

Steady target RWM amplitude coil current or error field

momentum conf. time  $\sim 1/\Omega (\tau_0 + i\tau_1) \rightarrow 1/(i\tau_1\Omega)$

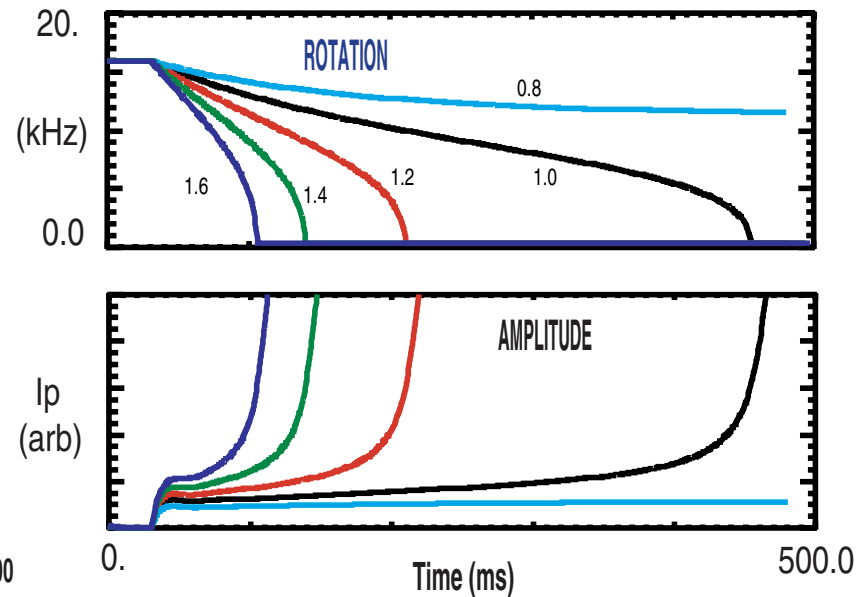
known as rotation dissipation "induction motor model"

## Experiment with Various External Fields



## Extended Lumped Parameter Model Simulation

Magnitude of External Field:  
0.8, 1.0, 1.2, 1.4, 1.8 (arb.)



# RWM Time Evolution with Extended Lumped Parameter Model Plus Angular Momentum Balance

- Example(2) : Active Magnetic Braking (Regulated rotation slowing down using mode amplitude controlled by feedback)

Steady target

RWM amplitude

coil current

$$\frac{d\theta}{dt} = \left( \frac{\omega_0}{m} \right) C_{vis} \operatorname{Im} \left[ \theta_p(t) \left( \theta_{c.fb}(t) + \theta_{c.pre.pro}(t) \right) \right]$$

momentum conf. time

$$\theta_p(t) = \frac{G_{fb}}{(1 - G_{fb})} \theta_{c.pre.pro}(t)$$

feedback gain



# RWM Time Evolution with Extended Lumped Parameter Model Plus Angular Momentum Balance

- Example(2) : Active Magnetic Braking (Regulated rotation slowing down using mode amplitude controlled by feedback)

$$\frac{d\Omega}{dt} = \left( \frac{C_{vis}}{m} \right) \text{Im}[\Omega_p(t) (\Omega_{c.fb}(t) + \Omega_{c.pre.pro}(t))] \quad \text{coil current}$$

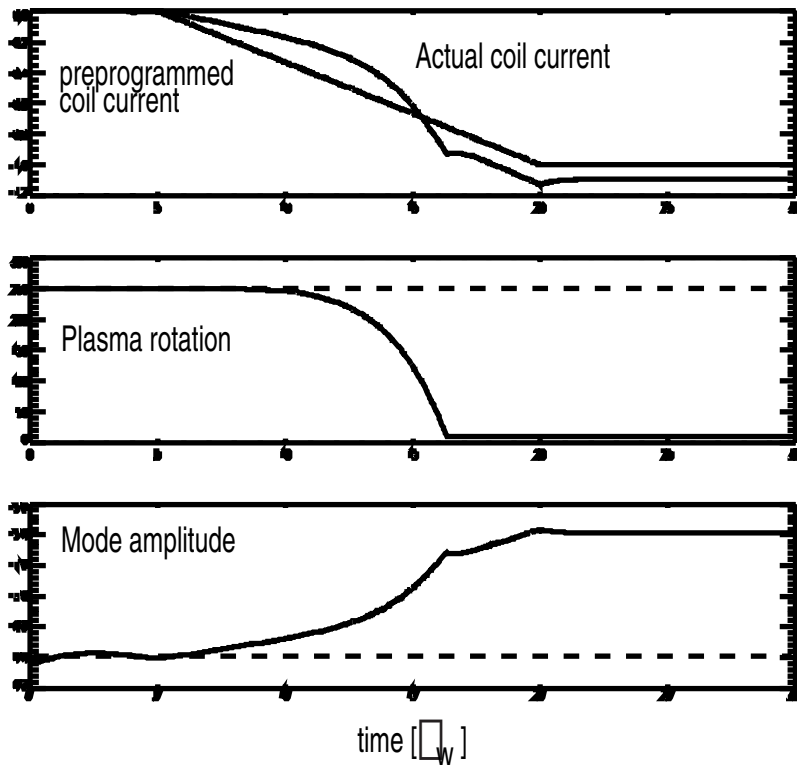
Steady target

RWM amplitude

momentum conf. time

$$\Omega_p(t) = \frac{G_{fb}}{(1 - G_{fb})} \Omega_{c.pre.pro}(t) \quad \text{feedback gain}$$

## Simulation



# RWM Time Evolution with Extended Lumped Parameter Model Plus Angular Momentum Balance

- Example(2) : Active Magnetic Braking (Regulated rotation slowing down using mode amplitude controlled by feedback)

$$\frac{d\alpha}{dt} = \left( \frac{1}{\tau_0} - \frac{C_{vis}}{m} \operatorname{Im}[\alpha(t) \rho_c(t) + \alpha(t) I_{c.pre.pro}] \right)$$

Steady target  $\rightarrow$   $\frac{1}{\tau_0}$  (momentum conf. time)

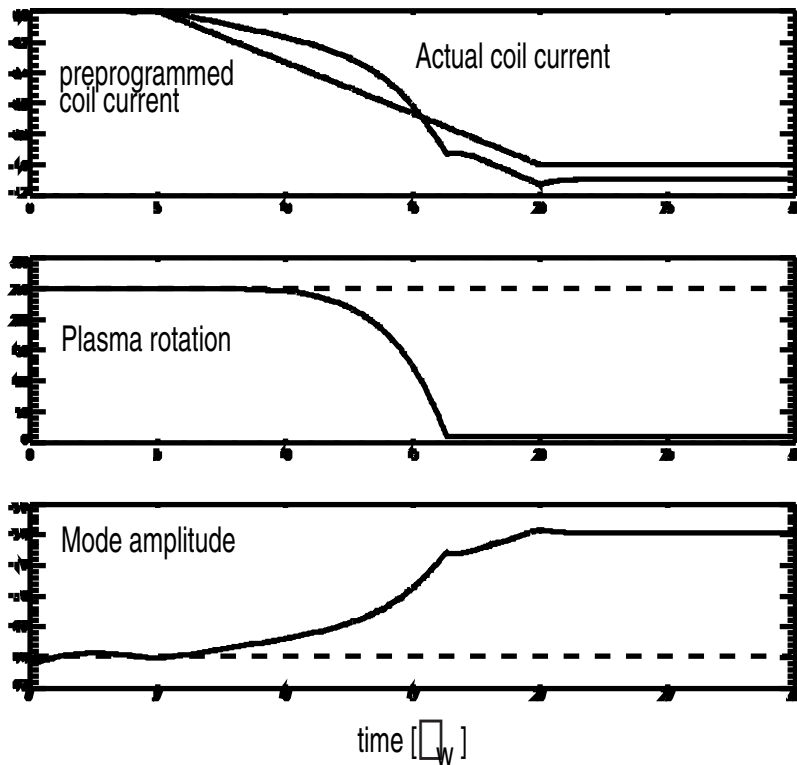
RWM amplitude  $\rightarrow$   $\alpha(t)$

coil current  $\rightarrow$   $I_{c.pre.pro}$

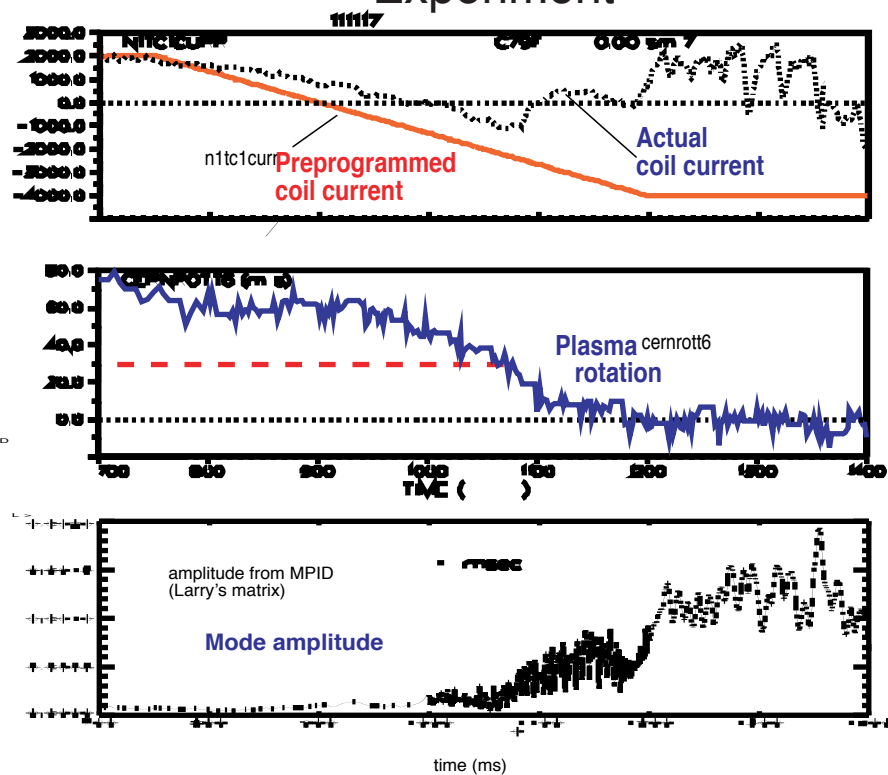
$$\alpha(t)_p = \frac{G_{fb}}{(1 - G_{fb})} \alpha(t)_{c.pre.pro}$$

feedback gain  $\rightarrow$   $G_{fb}$

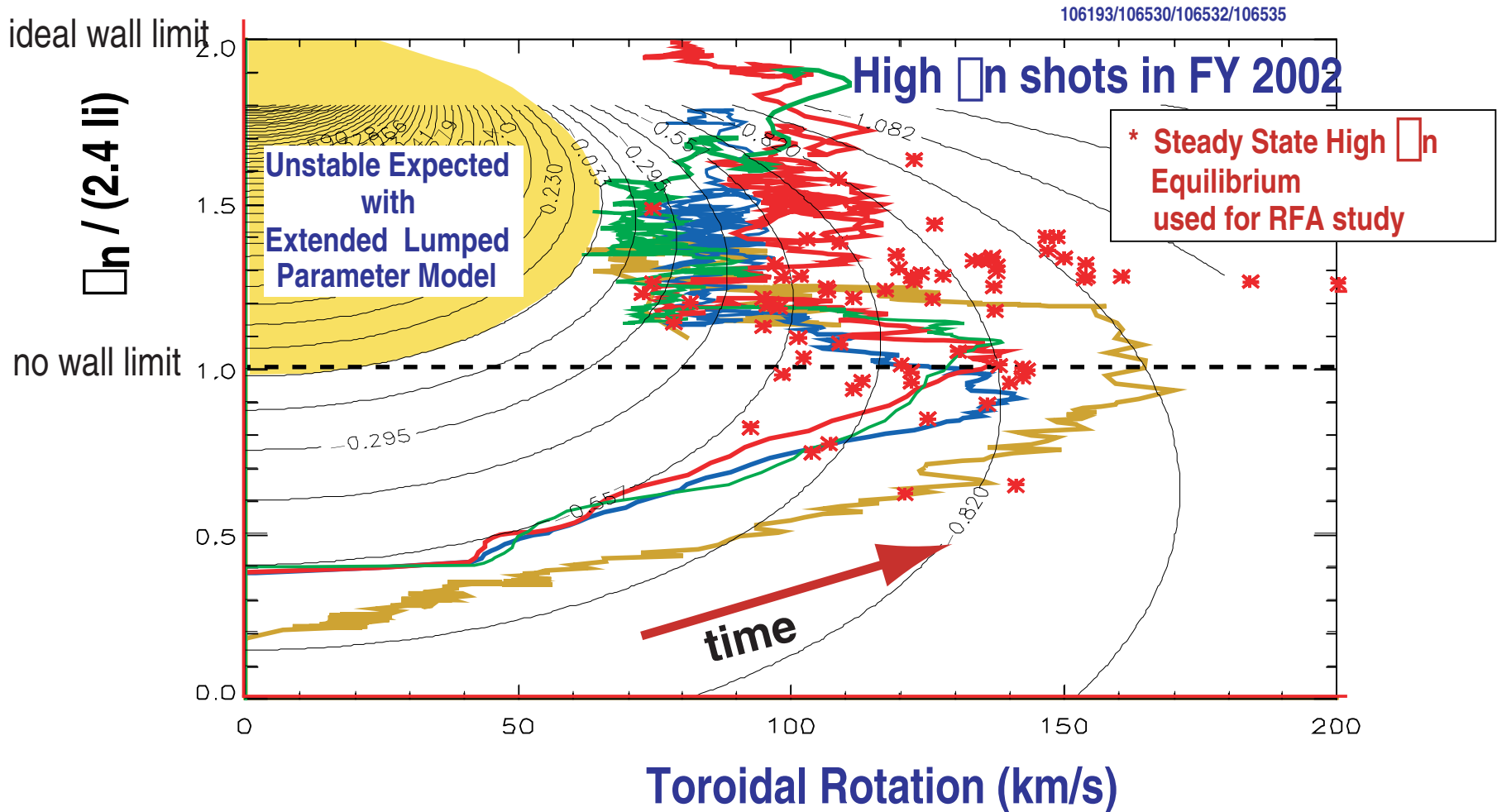
Simulation



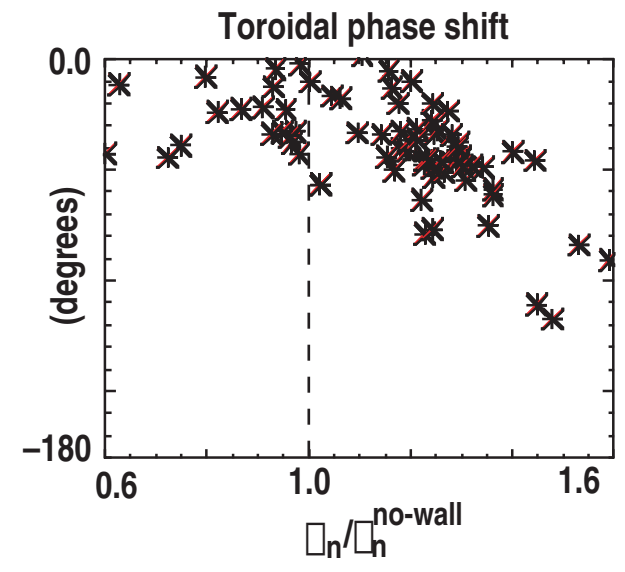
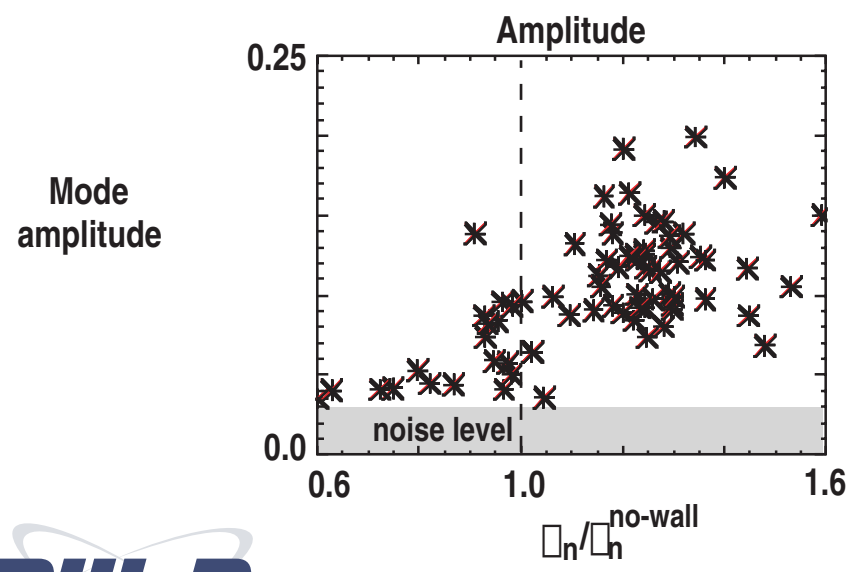
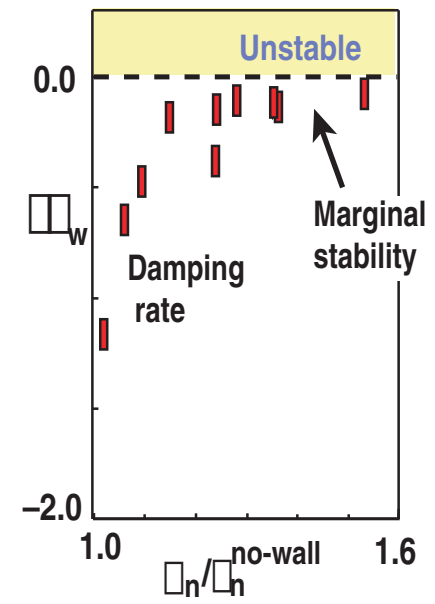
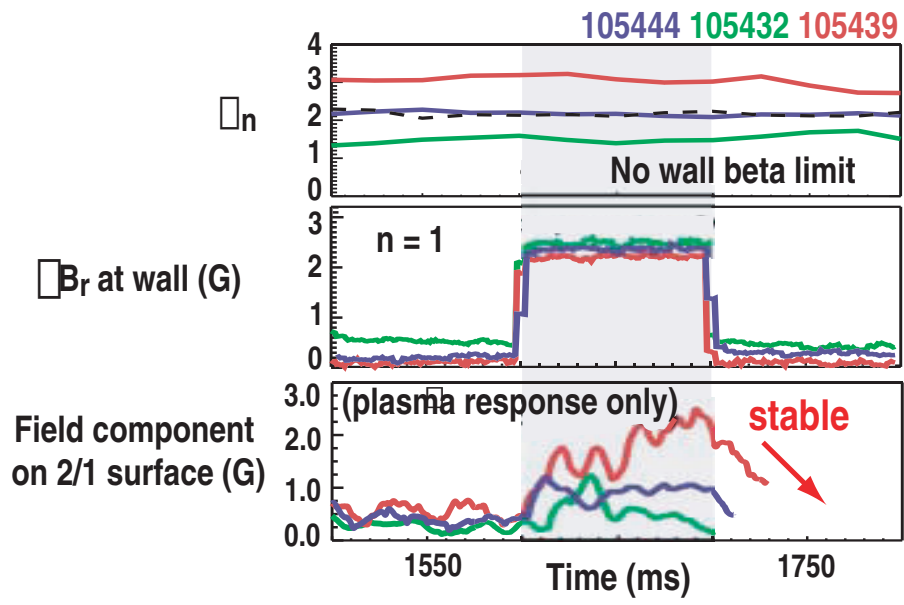
Experiment



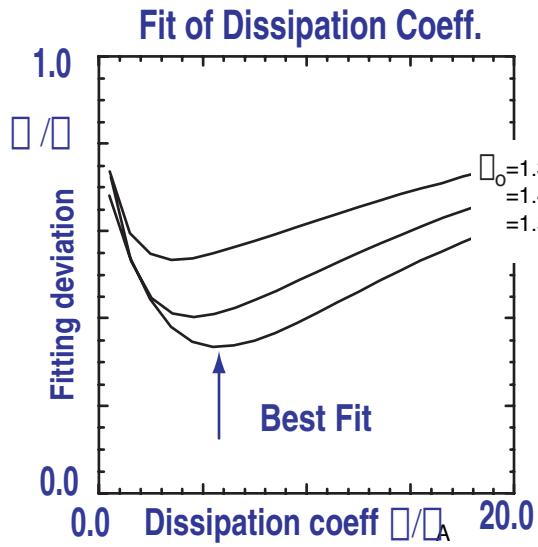
# STABLE REGIME PREDICTED BY EXTENDED LUMPED PARAMETER MODEL IS CONSISTENT WITH EXPERIMENTALLY ACHIEVED PARAMETERS



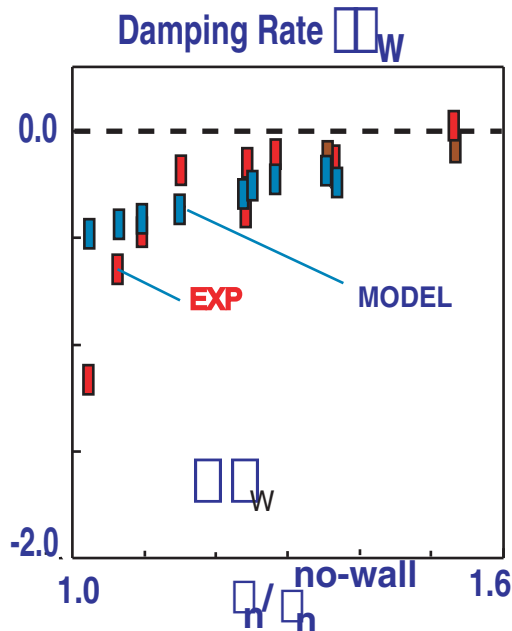
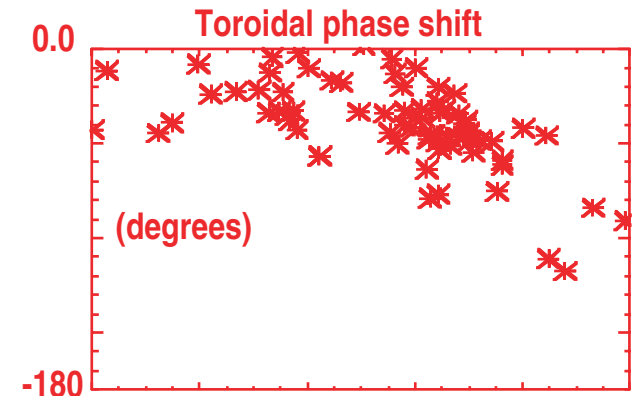
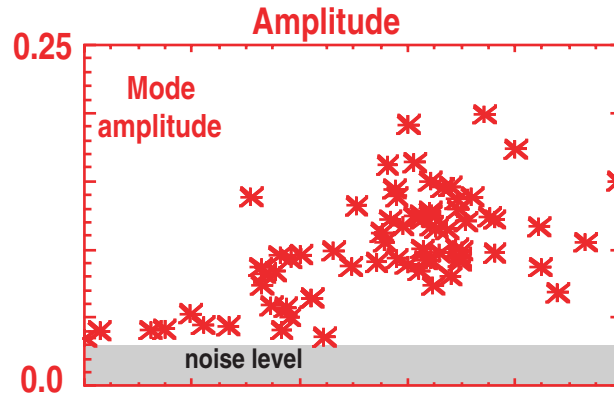
# RFA AMPLITUDE AND PHASE SHIFT INCREASE WITH INCREASE OF $\beta_n$ TO MARGINAL STABILITY



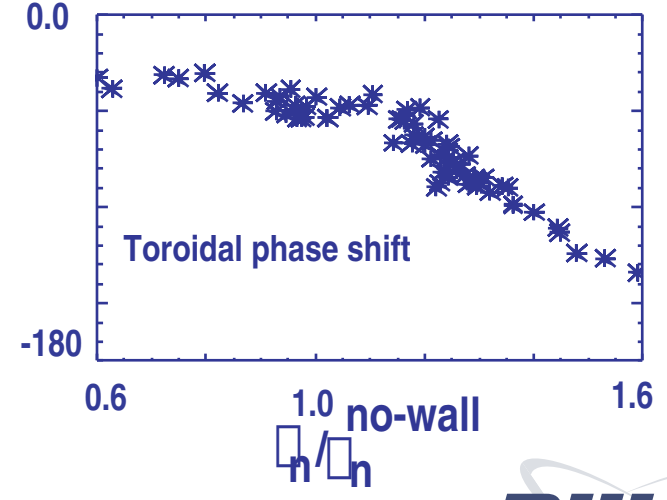
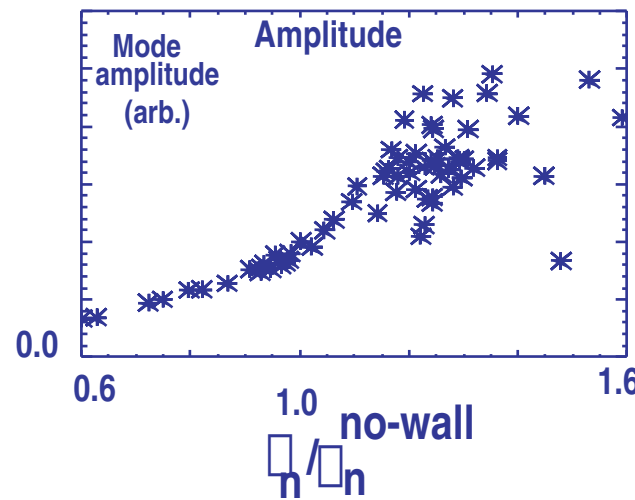
# COMPARISON OF MODEL AND OBSERVATIONS SHOWS THAT DAMPING OF RFA ARISES FROM ROTATIONAL DISSIPATION



## Observed Plasma Response to

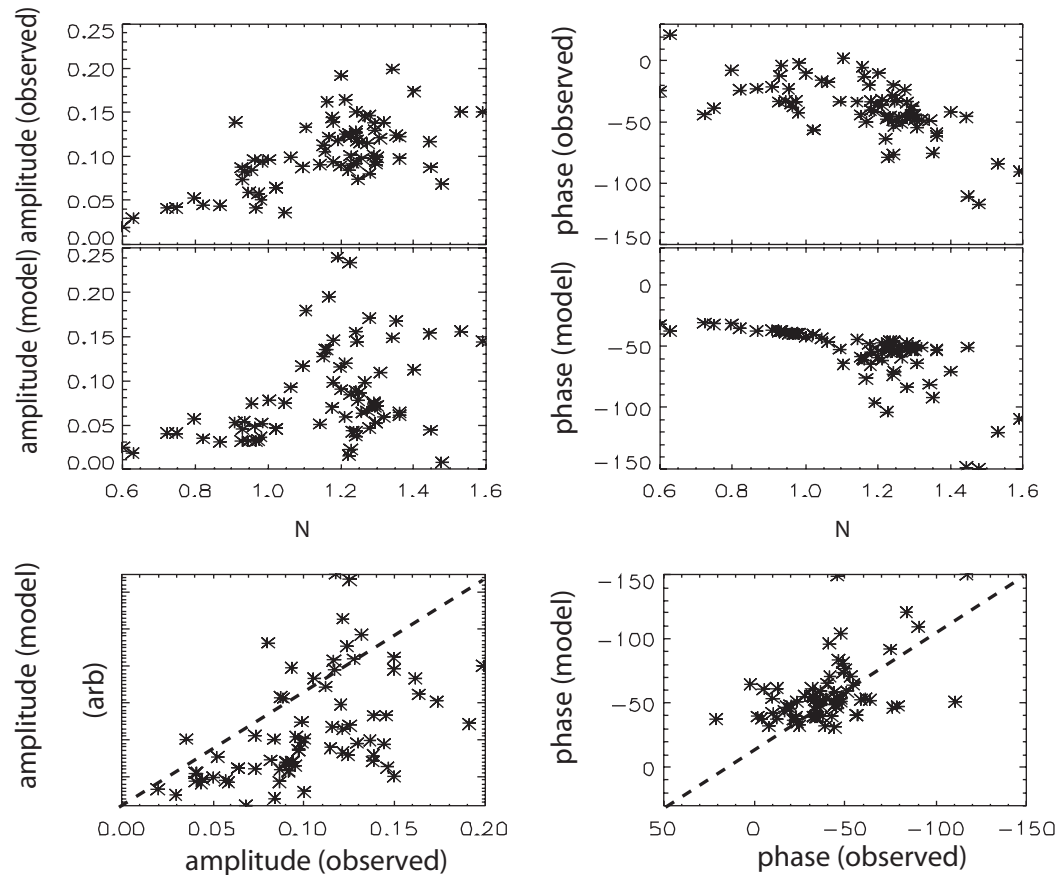


## Best fit to the model with the dissipation parameter $\gamma/\omega_A = 5$ .



• dissipation / damping rate :  $\gamma/\omega_n$  |  $\gamma_{exp}/\omega_w$  | 0.5 - 2

# COMPARISON OF LUMPED PARAMETER MODEL WITH EXPERIMENT



$$A = \frac{[\mathbf{W}_{IW}(\varphi = 0) + \varphi\varphi^2] + \varphi\varphi\varphi}{[\mathbf{W}_{nW}(\varphi = 0) + \varphi\varphi^2] + \varphi\varphi\varphi} \quad (14)$$

Qualitative agreement is also obtained by using the present lumped parameter model with different forms for A. This indicates more details should be included in future comparisons

# SUMMARY

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- **Extended Lumped Parameter Model includes the essence of RWM physics**
- **The present approach is consistent with other approaches**
- **Comparison with experimental results provides semi-quantitative discussion of the present RWM understandings**

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