Plasma 2 Lecture 23-RWM: Kink Mode Modeling with a Resistive Wall **APPH E6102y Columbia University**

- 2.5 MW/m³ achieved in TFTR!
- Establishes basic "scientific feasibility", but power out ~ power in.
- Fusion self-heating, characteristic of a "burning plasma", to be explored in ITER.
- **Control** instabilities, disruptions & transients still T.B.D.
- Steady state, maintainability, highavailability still T.B.D.
- The technologies needed for net power still T.B.D.





(Ia) Hot-Ion Mode in limiter plasma; (Ib) Hot-ion H-Mode;

(II) Optimized shear; and (III) Steady-state ELMY-H Modes.

IDENTIFICATION OF EXTERNAL KINK MODES IN JET

G.T.A. HUYSMANS, T.C. HENDER^{*}, B. ALPER JET Joint Undertaking, Abingdon, United Kingdom

 * UKAEA/Euratom Fusion Association, Culham, Abingdon, United Kingdom

ABSTRACT. The 'outer mode' is one of the MHD modes that limits the fusion performance of the hot ion H mode discharges in JET. It has previously been proposed that the outer mode is a nonlinearly saturated external kink mode. This was based on the localization of the perturbation close to the edge as observed in soft X ray (SXR), electron temperature and electron density measurements. In addition, MHD stability calculations showed that the plasma edge is close to the ideal external kink stability boundary at the time when the outer mode is observed. The SXR data of the outer mode are compared with predictions based on the mode structure of the ideal n = 1 external kink mode. Excellent agreement is found, confirming the identification of the outer mode as an external kink mode.



FIG. 1. (a) DD reaction rate R_{DD} , stored energy W, neutral beam injection (NBI) power, D_{α} signal and central electron temperature T_{e0} , showing the effect of the outer mode between 12.8 and 13.1 s. (b) Expanded time trace, showing the outer mode growth on an outboard midplane Mirnov coil.

FIG. 3. Edge stability diagram for discharge 38675, showing the kink and ballooning stability limits in the edge pressure gradient, edge current density plane. The pressure gradient and the current density are taken at the $\psi = 0.97$ flux surface. The time trace of the edge plasma parameters of discharge 38675 is included.

FIG. 4. JET soft X ray system, showing the 197 lines of sight for cameras A to J and camera V.

ECE and reflectometer signals, are collected and processed through the JET Central Acquisition and Trig-

Identification of a Low Plasma-Rotation Threshold for Stabilization of the Resistive-Wall Mode

The plasma rotation necessary for stabilization of resistive-wall modes (RWMs) is investigated by controlling the toroidal plasma rotation with external momentum input by injection of tangential neutral beams. The observed threshold is 0.3% of the Alfvén velocity and much smaller than the previous experimental results obtained with magnetic braking. This low critical rotation has a very weak β dependence as the ideal wall limit is approached. These results indicate that for large plasmas such as in future fusion reactors with low rotation, the requirement of the additional feedback control system for stabilizing RWM is much reduced.

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- M. Takechi,¹ G. Matsunaga,¹ N. Aiba,¹ T. Fujita,¹ T. Ozeki,¹ Y. Koide,¹ Y. Sakamoto,¹ G. Kurita,¹ A. Isayama,¹ Y. Kamada,¹ and the JT-60 team
 - ¹Japan Atomic Energy Agency, Naka, Ibaraki-ken, 311-0193 Japan (Received 14 November 2006; published 1 February 2007)

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FIG. 2 (color online). The temporal evolution of plasma current and internal inductance (a), and stored energy and injection power of NBs (b) of the plasma for the critical rotation experiment of RWM.

Poloidal cross section of the plasma for FIG. 1 (color online). the RWM experiment.

FIG. 4 (color online). Temporal evolution of rotation profile for E46710 before disruption. The error in rotation velocity is ± 1.5 km/s at q = 2 and is smaller than the open circle.

FIG. 3 (color online). Waveforms of E46710(red) and E46743(blue). (a) β_N , (b) n = 1 radial magnetic fluctuation and (c) toroidal rotation at q = 2 measured by CXRS. The power of counter NBs (d), co NBs (e), and perpendicular NBs (f). The horizontal dotted lines are calculated critical β (a) and critical rotation (c), respectively.

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Overview of JT-60U results towards the establishment of advanced tokamak operation

N. Oyama¹ and the JT-60 Team

Japan Atomic Energy Agency, Naka, Ibaraki-ken 311-0193, Japan

E-mail: oyama.naoyuki@jaea.go.jp

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Figure 6. Time evolution of magnetic fluctuations for (*a*) EWM and (*b*) the RWM precursor. Upper figures in (*a*) and (*b*) show integrated mode amplitude of n = 1 fluctuation.

Global Kink Eigenmodes

V24=0 V2X =0

PLASMA? WHAT FINE (46), XG) INSIDE AND OUTSIDE **Boundary conditions** VY = 0 (NO CURRENT) OUTSIDE PLASMA VY=0 (NO FLOW, VONTICITY, NOSRIA) (no CURRENTS INSIDE PLASMA TOO) (NO VORTICITY WITHIN PLASMA) PERTURSES FIELOS + PLANA MOTION DUT NO CORRENTS OR VORTICITY WITH WACL NOWALL $\psi(n) - \left(\frac{n}{a}\right)^m nca - \left(\frac{n}{a}\right)^m nca$ $\left(\frac{a}{n}\right)^{m} n \leq a \qquad \sim \frac{\left(\frac{b}{a}\right)^{m} - \left(\frac{a}{b}\right)^{m}}{\left(\frac{b}{a}\right)^{m} - \left(\frac{a}{b}\right)^{m} - \left(\frac{b}{b}\right)^{m}}$ $\overline{V}_{1} = \frac{2}{2} \times \nabla \mathbf{X} = \hat{\Theta} \frac{m}{n} \left(\frac{n}{a}\right)^{m} - \hat{\eta} \frac{im}{n} \left(\frac{n}{a}\right)^{m} insiso$ = $-\hat{\Theta} \frac{m}{n} \left(\frac{a}{n}\right)^{n} - \hat{\eta} \frac{im}{n} \left(\frac{a}{n}\right)^{n} = \hat{\Theta} \frac{m}{n} \left(\frac{a}{n}\right)^{n} \hat{\Theta} = \hat{\Theta} \frac$

Kink Mode

 $-\omega \hat{\psi}_{a} = \frac{B\rho}{2} (m - m\tau) \tilde{\lambda}_{a}$ $Gg\frac{2\chi}{2n} = \frac{2mBp}{4ma^2} \tilde{\psi}_a \left(\frac{-\Delta'(a)}{2m/a}\right)^{-1}$

GLOBAL KINK MODES Mal

 $\Delta'(a) = -\frac{m}{a}(\Lambda + 1)$ SHAFRANOU'S FURMULA

 $\Delta'(a) = -\frac{2m}{a} \frac{(b/a)^m}{(b/a)^m - (\frac{a}{b})^n} \quad \text{For } A \quad \text{where } A = b$ $\begin{cases} \overline{\lambda}_a & -\frac{b}{a} \\ \overline{\lambda}_a \\ \overline{\lambda}_a \\ \overline{\lambda}_a \\ \overline{\lambda}_a \\ \overline{\lambda}_a \end{cases} = -\frac{m}{a} \widetilde{\lambda}_a$ $\begin{aligned} \left\{ \omega^2 = 2 \omega_q^2 \left(m - nq \right) \\ \times \left[\left(m - nq \right) \left(\frac{\Lambda + 1}{2} \right) - 1 \right] \end{aligned}$ $\left(\begin{array}{ccc} & & & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & &$ $\cdot \lambda$ STARL

Wesson's Kink Modes LINEARIZED EQUATIONS FOR PERTURSED STREAM FUNCTION (X) AND PETTURSED PULLION FLUX (4) $-9\omega\nabla_{1}^{2}\overline{X}=-\frac{m}{n}\frac{2J_{2}}{\partial n}\overline{\psi}+\frac{Bp}{4m}(m-mg)\overline{D}_{1}^{2}\overline{\psi}$ putio) (induction) $-\omega \widehat{\psi} = \frac{R_{p}}{2} (m - m_{q}) \widetilde{\chi}$ LET'S TARK Q= UNIFORM, WITH A SHARP JUMP AT THE EDEE. $\left[\begin{array}{c} D = \frac{2X}{2n} \right] = \frac{B_{f}(a)}{M_{0}a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) \overline{\Psi}_{a} \left(\begin{array}{c} \Delta'(a) \\ \Delta'(a) \\ m \end{array} \right) = \frac{\Delta'(a)}{M_{0}a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) \overline{\Psi}_{a} \left(\begin{array}{c} \Delta'(a) \\ \Delta'(a) \\ m \end{array} \right) = \frac{\Delta'(a)}{M_{0}a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) \overline{\Psi}_{a} \left(\begin{array}{c} \Delta'(a) \\ \Delta'(a) \\ m \end{array} \right) = \frac{\Delta'(a)}{M_{0}a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) \overline{\Psi}_{a} \left(\begin{array}{c} \Delta'(a) \\ \Delta'(a) \\ m \end{array} \right) = \frac{\Delta'(a)}{M_{0}a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) \overline{\Psi}_{a} \left(\begin{array}{c} \Delta'(a) \\ \Delta'(a) \\ m \end{array} \right) = \frac{\Delta'(a)}{M_{0}a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) \overline{\Psi}_{a} \left(\begin{array}{c} \Delta'(a) \\ \Delta'(a) \\ m \end{array} \right) = \frac{\Delta'(a)}{M_{0}a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) \overline{\Psi}_{a} \left(\begin{array}{c} \Delta'(a) \\ \Delta'(a) \\ m \end{array} \right) = \frac{\Delta'(a)}{M_{0}a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) \overline{\Psi}_{a} \left(\begin{array}{c} \Delta'(a) \\ \Delta'(a) \\ m \end{array} \right) = \frac{\Delta'(a)}{M_{0}a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) \overline{\Psi}_{a} \left(\begin{array}{c} \Delta'(a) \\ \Delta'(a) \\ m \end{array} \right) = \frac{\Delta'(a)}{M_{0}a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) \overline{\Psi}_{a} \left(\begin{array}{c} \Delta'(a) \\ \Delta'(a) \\ m \end{array} \right) = \frac{\Delta'(a)}{M_{0}a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) \overline{\Psi}_{a} \left(\begin{array}{c} \Delta'(a) \\ \Delta'(a) \\ m \end{array} \right) = \frac{\Delta'(a)}{M_{0}a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) \overline{\Psi}_{a} \left(\begin{array}{c} \Delta'(a) \\ \Delta'(a) \\ m \end{array} \right) = \frac{\Delta'(a)}{M_{0}a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) \overline{\Psi}_{a} \left(\begin{array}{c} \Delta'(a) \\ \Delta'(a) \\ m \end{array} \right) = \frac{\Delta'(a)}{M_{0}a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) \overline{\Psi}_{a} \left(\begin{array}{c} \Delta'(a) \\ \Delta'(a) \\ m \end{array} \right) = \frac{\Delta'(a)}{M_{0}a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) \overline{\Psi}_{a} \left(\begin{array}{c} \Delta'(a) \\ \Delta'(a) \\ m \end{array} \right) = \frac{\Delta'(a)}{M_{0}a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) \overline{\Psi}_{a} \left(\begin{array}{c} \Delta'(a) \\ \Delta'(a) \\ \Delta'(a) \\ \Delta'(a) \end{array} \right) = \frac{\Delta'(a)}{M_{0}a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) \overline{\Psi}_{a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) = \frac{\Delta'(a)}{M_{0}a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) = \frac{\Delta'(a)}{M_{0}a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) = \frac{\Delta'(a)}{M_{0}a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) = \frac{\Delta'(a)}{M_{0}a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) = \frac{\Delta'(a)}{M_{0}a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) = \frac{\Delta'(a)}{M_{0}a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) = \frac{\Delta'(a)}{M_{0}a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) = \frac{\Delta'(a)}{M_{0}a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) = \frac{\Delta'(a)}{M_{0}a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) = \frac{\Delta'(a)}{M_{0}a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) = \frac{\Delta'(a)}{M_{0}a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) = \frac{\Delta'(a)}{M_{0}a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) = \frac{\Delta'(a)}{M_{0}a} \left(\begin{array}{c} m - mg_{a} \end{array} \right) = \frac{\Delta'(a)}{M_{0}a} \left(\begin{array}{c} m - m$ AT RASand's Edge WITH INDUCTION EQUATION: $\begin{aligned} & \left(\omega^2 = -\omega_A^2 \left(m - m g_a \right)^2 \Delta'(a) \frac{\partial a}{2\chi_A} \\ & \left(m - m g_a \right)^2 \Delta'(a) \frac{\partial a}{2\chi_A} \\ & \left(m - m g_a \right)^2 \Delta'(a) \frac{\partial a}{2\chi_A} \\ & \left(m - m g_a \right)^2 \Delta'(a) \frac{\partial a}{2\chi_A} \end{aligned}$ INSTABILITY REQUIRES ((a))0

PLASMAS EDSE:

DUT, HOW TO FIGURO OJT (()) (LILLLLLLLLL

SINCO [W] < WA, THE KINK MODE CAUSES THE INTERNAL " PLASMA TO RESPOND "QUICKLY" SO QUICKLY THAT WE CAN 19NOND THE TIMO CT TAMÁS TO FORM A DISTORTES, JD, QUASI-EQUILIANUM

INSIDE, THE PLASMA IS A "FORCES" EDUIJBACUN

 $O \approx -\frac{m}{n} \frac{\partial J_z}{\partial n} \widetilde{\varphi} + \frac{B_p}{mon} (m - m_g) V_1^2 \widetilde{\varphi}$

OUTSIDE, THE RESPONSE IS THE "UACUUM" RESPONSE.

WITH J2(n), WE HAVE TO SOLVE FOR & USING a Computin (This is UERY EASY FOR THE CELLINDICA "TOEducte")

Wesson's Kink Modes

With a "vacuum" and "perfectly conducting" exterior boundary.

- HAVE $\widehat{\Psi}(1=b) = 0$ i.e. $\widehat{\eta} \cdot \widehat{\pi} = 0$
- THE GALL ON A 'LONG" TIME SCALE

CURRENTS FLOW ON THEIR SUNFACES

Resistive Wall Modes

· EXTERNAL KINFS WITH A PERFECTLY CONSULTING (IDEAL) WALL

· WITH A RESISTIVE WALL, THE NORMAL FIELD DIFRISES THROUGH

 $\Delta'(a) \widehat{\Psi}(a) = M_0 K_2(\theta, \varphi) \in SURFACE SURNERT AT N=a$ $\Delta'(b) \varphi(b) = \mu_{s} K_{2}^{W}(\theta, \varphi) \leftarrow SURFACE CURRENT AT \eta = b$

Cylindrical Form of Perturbed Magnetic Flux $= \hat{\partial} \frac{24}{2\pi} - \frac{i \hat{n} \hat{m} \hat{\varphi}}{2\pi} \qquad \left(\hat{n} < c \right)$

$$\overline{B} = \widehat{i} \times \nabla \Psi = \widehat{\partial} \frac{2\Psi}{2\pi} - \widehat{i}_{\pi} \left(\frac{2\Psi}{2\theta} \right)$$

Ý = CONSTANT ACNOSS CURRENT LAYER =) B-M=0

$$\Delta' = \frac{1}{\varphi} \left(\frac{2 + 1}{2 + 1} - \frac{2 + 1}{2 + 1} \right) \neq 0$$

$$\Psi(h) = \begin{cases} \Psi_a \left(\frac{\pi}{a}\right)^m & n < a \\ \Psi_a \left(\frac{\pi}{b}\right)^n - \left(\frac{b}{a}\right)^n \\ \Psi_a \left(\frac{\pi}{b}\right)^n - \left(\frac{b}{a}\right)^n \\ \Psi_a \left(\frac{b}{a}\right)^n - \left(\frac{b}{a}\right)^n \\ \Psi_b \left(\frac{b}{a}\right)^m \\$$

$$\Lambda'(a) = \frac{1}{\varphi_{a}} \left(\frac{2t}{z_{1}} - \frac{2t}{z_{1}} \right)$$

$$\Delta'(B) = \frac{1}{\varphi} \left(\frac{24}{2} - \frac{24}{2} \right)$$

UHEN THENS EXISTS 4 PERTURSES CURRENT

KY * NOTE: THIS CHANGES INSIDE A PLASMA

 $\int = \frac{2m}{b} \frac{1}{1-c} + \frac{\sqrt{c}}{1-c} \frac{2m}{b} \frac{\sqrt{a}}{\varphi}$ 15

Cylindrical Form of Perturbed Magnetic Flux

"EFFECT OF CONSULTION LAW"

ALLAYS STABILITING

 $c = \left(\frac{a}{b}\right)^{2}$

Since A'(a) > 0 For INSTASILITY 16

Resistive Relaxation of Wall Eddy Currents

ジェレジキ=-レ×カテ $\nabla \times (224) = \nabla \times \pi \overline{J}$ $= \frac{m}{\mu_{0} \partial \omega} \Lambda'(b) \tilde{\Psi}(b)$

OR

External Kink and Resistive Wall Mode

SHAFRANOU EQUILIBRIUN

 $\frac{d\psi_{a}}{dt} = \frac{B\rho}{e} i (m - mq) \cdot \tilde{\chi}_{a}$ $\int \frac{d\psi_{a}}{dt} = \frac{2mB\rho}{\mu_{a}e} \left[(m - mq) \frac{\Delta'(e)}{(2m/e)} + 1 \right] \psi_{a}$ $\int \frac{d\tilde{\chi}_{a}}{dt} = i \frac{2mB\rho}{\mu_{a}e} \left[(m - mq) \frac{\Delta'(e)}{(2m/e)} + 1 \right] \psi_{a}$ $\int_{\Delta} \frac{d^2 \hat{\psi}_a}{dt^2} = -2 \omega_A^2 \left(m - ng\right) \left[\left(m - ng\right) \frac{\Delta' \left[a\right]}{R - q_a} + 1 \right] \hat{\psi}_a$

PLASMA DYNAMICS

 $\frac{d^{2}\hat{\psi}_{a}}{dt^{2}} = -2\omega_{A}^{2}\left(m-n_{e}\right)^{2}\frac{c}{1-c}\left[\frac{\hat{\psi}_{b}}{\nabla e} + \frac{\int_{1-c}^{1-c} -\frac{1}{c}\hat{\psi}_{a}}{c(m-n_{e})} - \frac{1}{c}\hat{\psi}_{a}\right]$

External Kink and Resistive Wall Mode

WESSON" EQUILIBRIUM

 $\omega^{2} = -\omega_{A}^{2} \left(m - m q_{a} \right)^{2} \Delta^{\prime}(a) \frac{\chi_{a}}{2\chi_{a}}_{a}^{a} - \frac{\chi_{a}}{2} \int_{a}^{a} \int_{a}$

General RWM Dynamics w No Flow/No Dissipation

THORE ROUTS

- ROSTI = STASLA ALFUEL WAVE
- ROOT 2 = EXTERNETING MODE CONTLES TO UALL
- ROOT] = WALL MODE

2 ELSEN VECTORS

20

Usual "RWM Limit"

THEN: "PLASMA INFRITIA" IS 19NORAD

OR

 $(1-5)\overline{\varphi}_{a} = \overline{\varphi}_{a}/\overline{v}_{c}$

 $\frac{d\hat{\psi}_{0}}{dt} \neq \underbrace{\nabla_{u}}_{1-c}\hat{\psi}_{0} = \underbrace{\nabla_{u}}_{1-c}\underbrace{\nabla_{u}}_{c}\hat{\psi}_{1-c} = \underbrace{\nabla_{u}}_{(1-c)(1-\bar{s})}$

* .

 $\frac{1}{21} \int \frac{\overline{5}}{(1-\overline{5})(1-\overline{c})} \left(\frac{1}{(1-\overline{c})} \right) \left(\frac{1}{(1-\overline{c})} \right) \left(\frac{1}{(1-\overline{c})} \right) \left(\frac{1}{(1-\overline{c})} \right)$

(Nuc Fusion 36 (1996) pp. 11)

Fitzpatrick-Aydemir Model STABILIZATION OF THE RESISTIVE SHELL MODE IN TOKAMAKS

R. FITZPATRICK, A.Y. AYDEMIR Institute for Fusion Studies The University of Texas at Austin, Austin, Texas, United States of America

ABSTRACT. The stability of current-driven external-kink modes is investigated in a tokamak plasma sur rounded by an external shell of finite electrical conductivity. According to conventional theory, the ideal mode can be stabilized by placing the shell sufficiently close to the plasma, but the non-rotating 'resistive shell mode' which grows as the characteristic L/R time of the shell, always persists. It is demonstrated, using both analytic and numerical techniques, that a combination of strong edge plasma rotation and dissipation somewhere inside the plasma is capable of stabilizing the resistive shell mode. This stabilization mechanism is similar to that found recently by Bondeson and Ward, except that it does not necessarily depend on toroidicity, plasma compressibility or the presence of resonant surfaces inside the plasma. The general requirements for the stabilization of the resistive shell mode are elucidated.

Further Reading...

Simplified forms of the dynamical equations for the perturbed flux at the plasma edge, ψ_a , and the conducting wall, ψ_w , were summarized by Fitzpatrick [3] who also included the perturbed flux at the wall driven by control coils, ψ_c . The perturbed flux is related to perturbed radial magnetic field as

$$b_r(r,\theta,\phi,t) = \Re \left\{ i \frac{m}{r} \psi(r) e^{i(m\theta-\phi)+\gamma t} \right\}.$$

The three model equations describe an external kink mode coupled to a surrounding wall, the resistive dissipation of wall eddy currents, and toroidal torque balance. These equations are:

$$\frac{d^2\psi_a}{dt^2} + (\nu^* - 2i\Omega_\phi)\frac{d\psi_a}{dt} + \left[\gamma_{MHD}^2(1-\bar{s}) - \Omega_\phi^2 - i\nu^*\Omega_\phi\right]\psi_a = \gamma_{MHD}^2\frac{\psi_w}{\sqrt{c}}$$
$$\frac{d\psi_w}{dt} + \frac{\gamma_w}{1-c}\left(\psi_w - \sqrt{c}\psi_a\right) = \gamma_w\psi_c$$
$$\frac{d\Omega_\phi}{dt} + \nu^*(\Omega_\phi - \Omega_\phi^{(0)}) = -\frac{1}{2}\nu^*\Omega_\phi\frac{1+c}{1-c}\frac{|\psi_a|^2}{\delta M_a}$$

where c is a coupling coefficient between the wall and the plasma, $\bar{s} \equiv s/s_{crit} = s(1-c)/c$ is the normalized Boozer stability parameter, Ω_{ϕ} is the plasma rotation at the edge, ν^* is the (anomalous) viscosity, δM_a is the effective mass of the inertial layer, and L_p is the effective inductance of the perturbed plasma skin current. For a complete cylindrical wall, $c \approx (a/b)^{2m}$. VALEN [9] can be used to calculate c and γ_w for an incomplete wall, since c is related to the ideal wall stability limit through the definition $s_{crit} = c/(1-c)$ and since the resistive wall mode growth rate is proportional to γ_w when $0 < \bar{s} \ll 1$.

