Lecture 8: Plasma Physics 1

APPH E6101x Columbia University

Last Lecture (online)

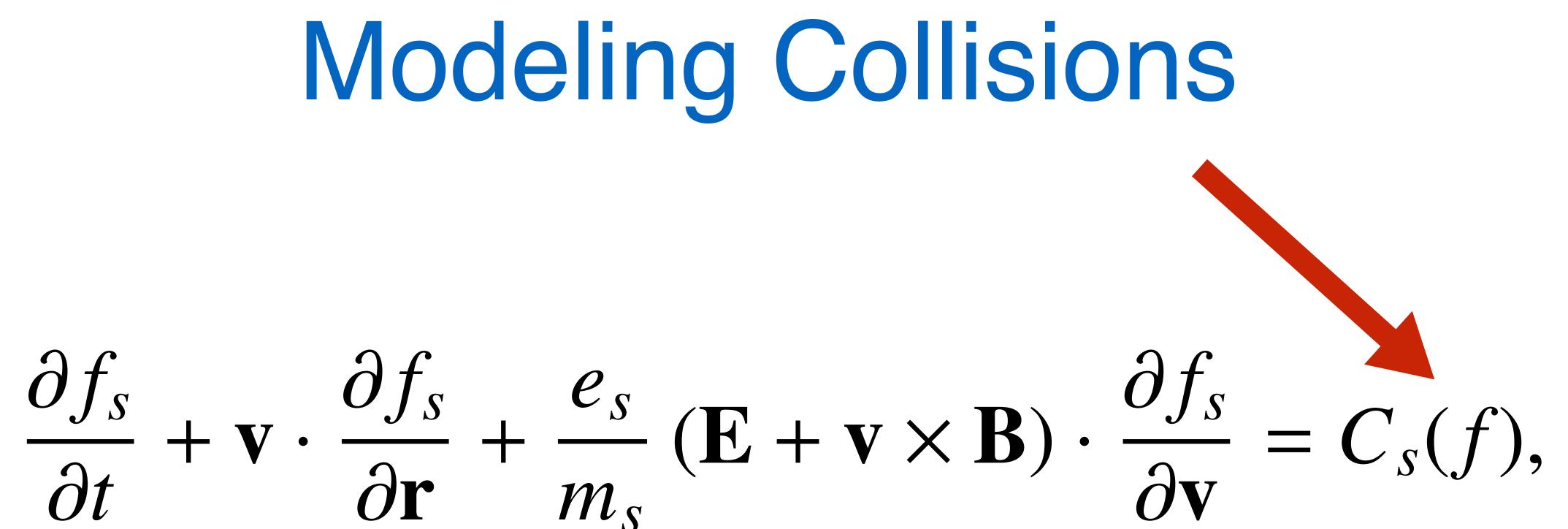
- Moments of the distribution function
- Fluid equations ("two fluid")
- The "closure problem"
- MHD equations ("single fluid")



- Homework #4: Modeling Collisions and the Rosenbluth Potentials
- Force balance (*equilibrium*) in a magnetized plasma
 - Z-pinch
 - θ-pinch
 - Screw-pinch (straight tokamak)
 - Grad-Shafranov Equation
- Conservation principles in magnetiz particles/flux tubes)

Conservation principles in magnetized plasma ("frozen-in" and conservation of

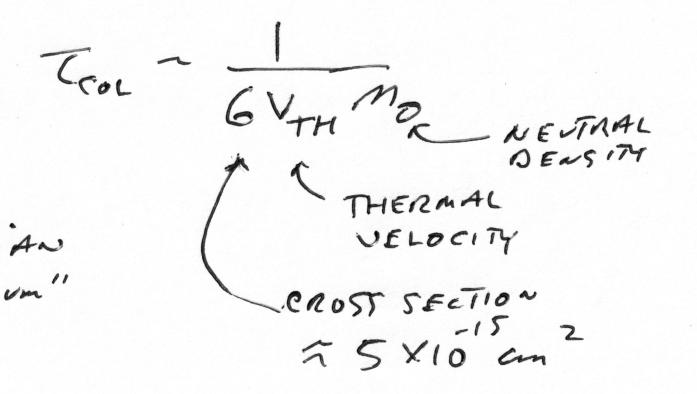
- "Weakly ionized plasma" collisions with neutrals
- Fully ionized plasma: Coulomb collisions

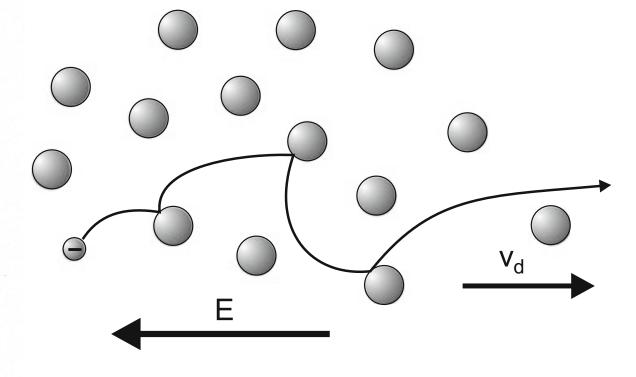


"Simple" Fixed-o Model for Weakly Ionized Plasma

 $C_{S}(F) \approx -\frac{1}{5}(F - f_{0})$ $T_{FOL} = \frac{1}{6V_{TH}}M_{0}$ MAXWELL-IAN PERTUNBED"EQUILIBRIUM" CROST SECTIONPERTUNBED DISTRIBUTION.

 $\iint d^3 v C_r(4) = 0$ $(\int \partial U \overline{U} C_{s}(s) = -\overline{V} M / \overline{L} Collision$ THEN 1D





$$(F < f_0 \overline{\upsilon}) = o)$$



Modeling Collisions in Fully Ionized Plasma

Rutherford scattering cross-section,

$$\frac{d\sigma}{d\Omega} = \frac{1}{4} \left(\frac{e_s e_{s'}}{4\pi \epsilon_0 \mu_{ss'} u_{ss'}^2} \right)^2 \frac{1}{s}$$

(Rutherford 1911). It is immediately apparent, from the previous formula, that twoparticle Coulomb collisions are dominated by small-angle (i.e., small χ) scattering events.

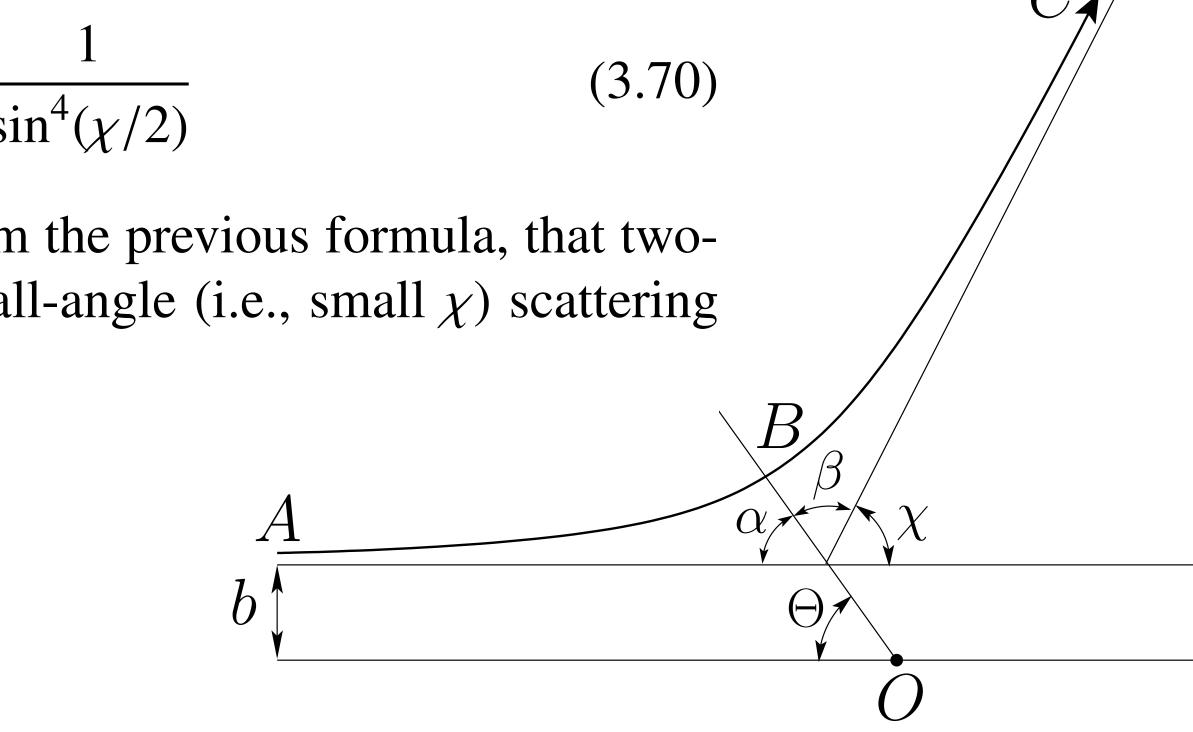


Figure 3.1 A two-body Coulomb collision.

Modeling Collisions in Fully Ionized Plasma

CURRENTS DRIVEN BY ELECTRON CYCLOTRON WAVES

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ABSTRACT. Certain aspects of the generation of steady-state currents by electron cyclotron waves are explored. A numerical solution of the Fokker-Planck equation is used to verify the theory of Fisch and Boozer and to extend their results into the non-linear regime. Relativistic effects on the current generated are discussed. Applications to steady-state tokamak reactors are considered.

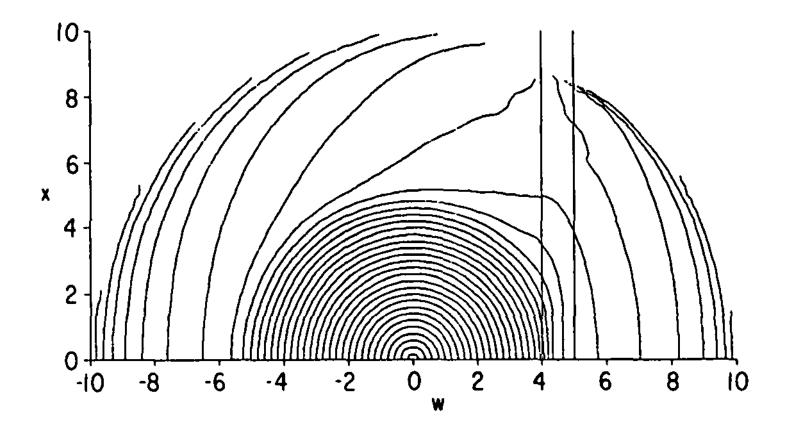


FIG.5. Steady-state distribution for D = 0.25, $w_1 = 4$, and $w_2 = 5$ (cyclotron damping).

https://doi.org/10.1088/0029-5515/21/12/004

Electron-cyclotron heating in a pulsed mirror experiment

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(Received 5 December 1983; accepted 6 August 1984)

Experimental measurements of electron-cyclotron resonance heating (ECRH) of a highly ionized plasma in mirror geometry is compared to a two-dimensional, time-dependent, Fokker–Planck simulation. Measurements of the absorption strength of the electrons and of the energy confinement of the ions helped to specify the parameters of the code. The electron energy distribution is measured with an end-loss analyzer and a target x-ray detector. These characterize a non-Maxwellian distribution consisting of "passing" (10 eV < $T_{e,p}$ < 30 eV), "warm" (50 eV < $T_{e,w}$ < 300 eV), and "hot" (1.2 keV < $T_{e,h}$ < 4.0 keV) electron populations. The temperature and fractional densities of the warm and hot populations depend on the absorbed power and total density. A similar distribution is calculated with the simulation program that reproduces the end-loss and x-ray signals. Both the experimental measurements and the simulation are described.

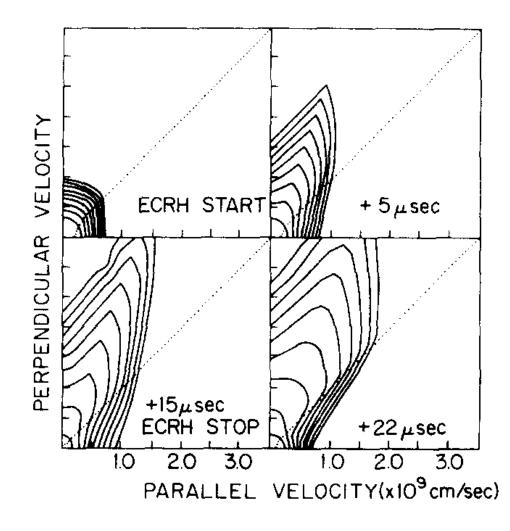


FIG. 9. An example of the development of the electron velocity distribution during and after ECRH. Shown are four times: (a) at the start of the ECRH, (b) after 5.0 μ sec, (c) at the end of the 15 μ sec rf pulse, and (d) 5.0 μ sec after the ECRH was turned off.

https://doi.org/10.1063/1.864605

Modeling Collisions in Fully Ionized Plasma $C_{ss'} = \iint u_{ss'} \frac{d\sigma}{d\Omega} \left(f'_s f'_{s'} - f_s f_{s'} \right) d^3 \mathbf{v}_{s'} d\Omega,$

$$\mathbf{v}_{s}' = \mathbf{v}_{s} + \frac{\mu_{ss'}}{m_{s}} \mathbf{g}_{ss'},$$

$$f_s(\mathbf{v}'_s) \simeq f_s(\mathbf{v}_s) + \frac{\mu_{ss'}}{m_s} \,\mathbf{g}_{ss'} \cdot \frac{\partial f_s(\mathbf{v}_s)}{\partial \mathbf{v}_s} + \frac{1}{2} \,\frac{\mu_{ss'}^2}{m_s^2} \,\mathbf{g}_{ss'} \,\mathbf{g}_{ss'} \,\mathbf{g}_{ss'} : \frac{\partial^2 f_s(\mathbf{v}_s)}{\partial \mathbf{v}_s \partial \mathbf{v}_s}$$

 $u_{ss'} = |\mathbf{V}_s - \mathbf{V}_{s'}|$

$$\mathbf{g}_{ss'} = \mathbf{u}_{ss'}' - \mathbf{u}_{ss'}$$



Modeling Collisions in Fully Ionized Plasma $C_{ss'} = \iint \left[u_{ss'} \frac{d\sigma}{d\Omega} \left(f'_s f'_{s'} - f_s f_{s'} \right) d^3 \mathbf{v}_{s'} d\Omega \right],$

 $f'_{s}f'_{s'} - f_{s}f_{s'} \simeq \mu_{ss'} \mathbf{g}_{ss'} \cdot \left(\frac{\partial f_{s}}{\partial \mathbf{v}_{s}} \frac{f_{s'}}{m_{s}}\right)$

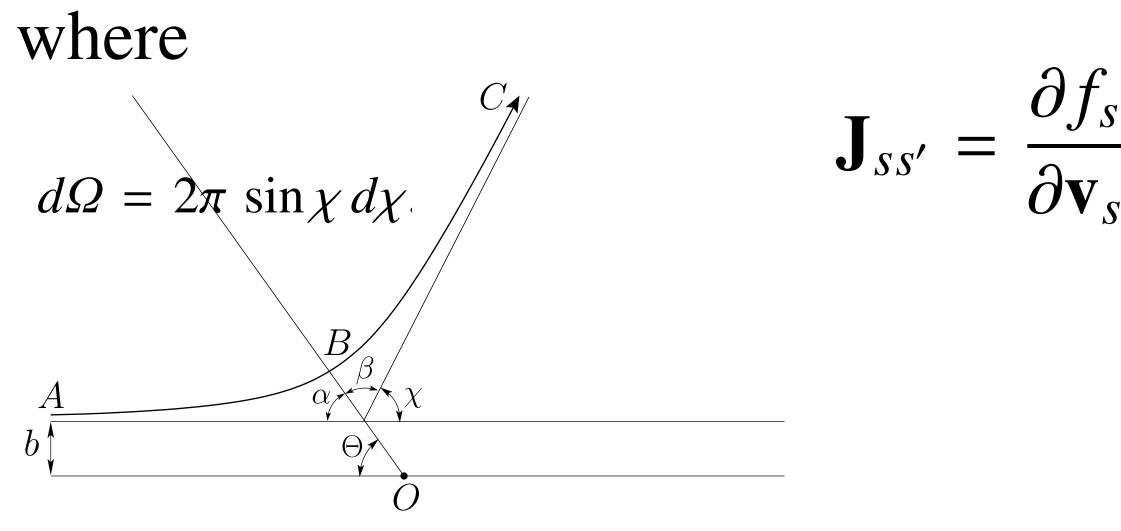
 $+\frac{1}{2}\mu_{ss'}^2 \mathbf{g}_{ss'}\mathbf{g}_{ss'} : \left(\frac{1}{\partial t}\right)$





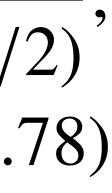
Modeling Collisions in Fully Ionized Plasma

$$C_{ss'} \simeq \frac{1}{4} \left(\frac{e_s e_{s'}}{4\pi \epsilon_0 \mu_{ss'}} \right)^2 \\ \times \int \int \left[\mu_{ss'} \mathbf{g}_{ss'} \cdot \mathbf{J}_{ss'} + \frac{1}{2} \mu_{ss'}^2 \mathbf{g}_{ss'} \mathbf{g}_{ss'} \mathbf{g}_{ss'} : \left(\frac{1}{m_s} \frac{\partial}{\partial \mathbf{v}_s} - \frac{1}{m_{s'}} \frac{\partial}{\partial \mathbf{v}_{s'}} \right) \mathbf{J}_{ss'} \right] \frac{d^3 \mathbf{v}_{s'} d\Omega}{u_{ss'}^3 \sin^4(\chi/\chi)}$$
(3.



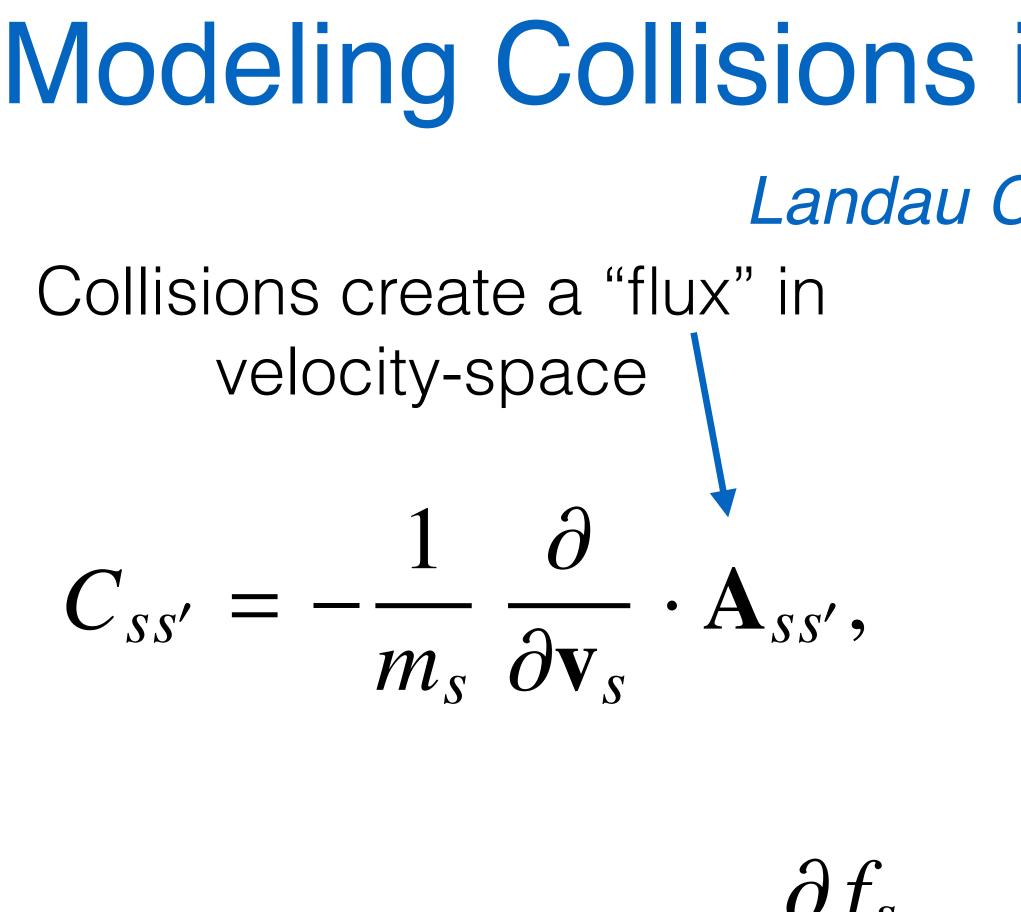
$$\frac{f_{s'}}{s} \frac{f_{s'}}{m_s} - \frac{f_s}{m_{s'}} \frac{\partial f_{s'}}{\partial \mathbf{V}_{s'}}.$$

 $\mathbf{g}_{SS'} = \mathbf{u}_{SS'}' - \mathbf{u}_{SS'}$





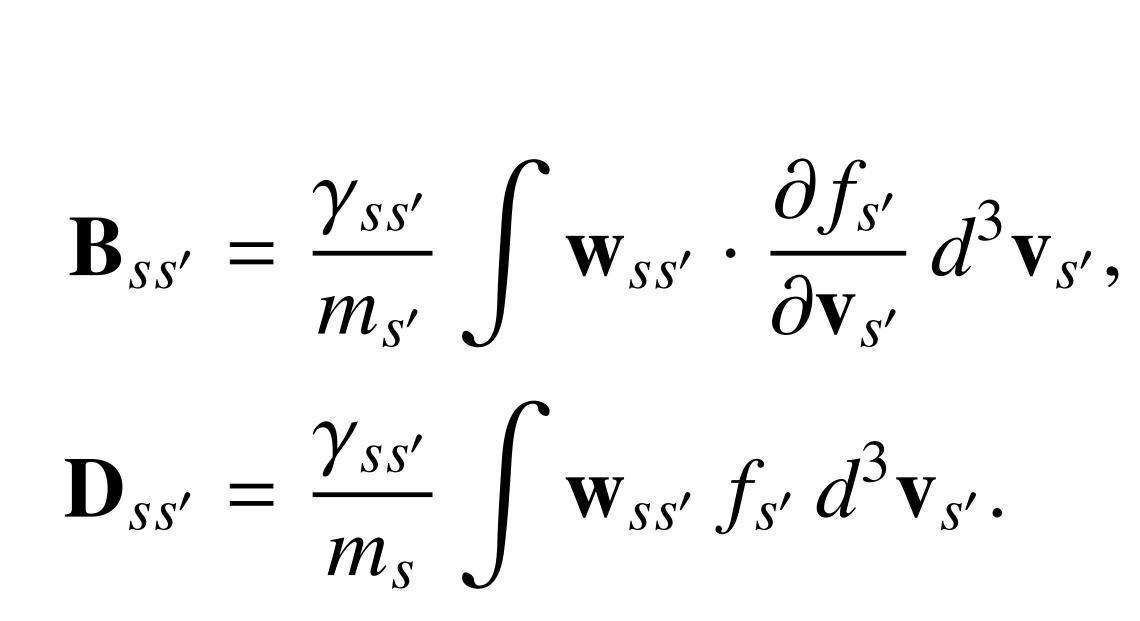




 $\mathbf{A}_{ss'} = \mathbf{B}_{ss'} f_s - \mathbf{D}_{ss'} \cdot \frac{\partial f_s}{\partial \mathbf{v}_s},$ "Diffusion" "Drag"

Modeling Collisions in Fully Ionized Plasma

Landau Collision Operator





Rosenbluth Potentials

 $\mathbf{B}_{ss'} = \frac{2\gamma_{ss'}}{m_{s'}} \frac{\partial H_{s'}}{\partial \mathbf{v}_s}, \quad G_{s'}(\mathbf{v}_s) = \int u_{ss'} f_{s'} d^3 \mathbf{v}_{s'},$ $\mathbf{D}_{ss'} = \frac{\gamma_{ss'}}{m_s} \frac{\partial^2 G_{s'}}{\partial \mathbf{v}_s \partial \mathbf{v}_s}. \quad H_{s'}(\mathbf{v}_s) = \int u_{ss'}^{-1} f_{s'} d^3 \mathbf{v}_{s'}.$ $\nabla_v^2 H_{s'} = -4\pi f_{s'}(\mathbf{v}),$ $\nabla_n^2 G_{S'} = 2 H_{S'}(\mathbf{v}),$

Rosenbluth Potentials

APPENDIX: NUMERICAL TECHNIQUES

Here we describe with more detail the numerical tech- is used with d to color the tor 1 montial agreetian **...** nique [Eq.

The

$$\begin{aligned} & \text{(32)] given by} \\ & \Gamma_{v} = \Gamma_{e\alpha} \left(1 - \frac{M_{e\alpha}}{m_{e}} \right) F \frac{\partial H}{\partial v} - \frac{\Gamma_{e\alpha}}{2} \\ & \frac{\partial F}{\partial v} - \frac{1}{v^{2}} \frac{\partial}{\partial v} v^{2} \Gamma_{v} - \frac{1}{v \sin \theta} \frac{\partial}{\partial \theta} \sin \theta \Gamma_{\theta}. \\ & \text{(A1)} \\ & \text{ff currents are given by Eqs. (17), (18), (29), and (30), or} \\ & \Gamma_{v} = |\cos \theta| (\Gamma_{E}/L), \\ & \Gamma_{\theta} = \frac{B}{\sin \theta} \left(\frac{1}{R_{res}} - \sin^{2} \theta \right) \frac{\Gamma_{E}}{L}. \end{aligned}$$

$$\begin{aligned} & \Gamma_{v} = (A2) \\ & (A2) \end{aligned}$$

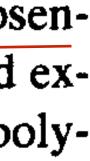
$$\begin{aligned} & \Gamma_{v} = \Gamma_{e\alpha} \left(1 - \frac{M_{e\alpha}}{m_{e}} \right) F \frac{\partial H}{\partial v} - \frac{\Gamma_{e\alpha}}{2} \\ & \times \left[\frac{\partial^{2} G}{\partial v \partial \theta} - \frac{\partial G}{\partial v \partial \theta} \right] \frac{\partial F}{\partial \theta} \right], \\ & \times \left[\frac{1}{v^{2}} \left(\frac{1}{v} \frac{\partial^{2} G}{\partial \theta^{2}} + \frac{\partial G}{\partial v} \right) \frac{\partial F}{\partial \theta} - \frac{1}{v} \frac{\partial^{2} G}{\partial v \partial \theta} \frac{\partial F}{\partial v} \right], \end{aligned}$$

https://doi.org/10₃1063/1.864605

For the collisional currents, the form used by Cutter et al.²⁰

where $\Gamma_{e\alpha} = 4\pi e^2 e_{\alpha}^2 \lambda_{e\alpha} / m_e^2$. Here H and G are the Rosenbluth potentials which are approximated by a truncated expansion of spherical harmonics.²⁰ The first seven, even poly-



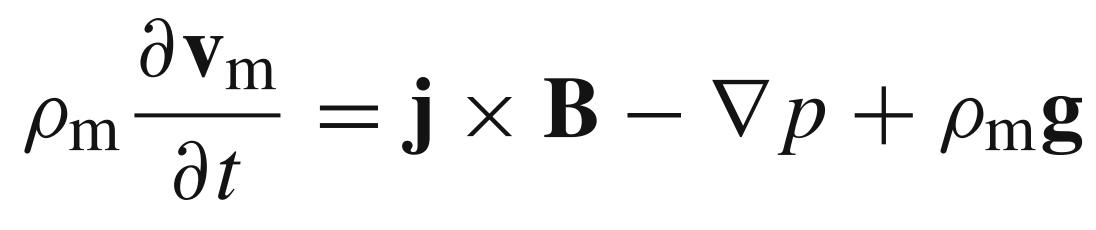




- Homework #4: Modeling Collisions and the Rosenbluth Potentials
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Conservation principles in magnetized plasma ("frozen-in" and conservation of





$\mathbf{E} + \mathbf{v}_{\mathrm{m}} \times \mathbf{B} = \eta \mathbf{j} + \frac{1}{ne} (\mathbf{j} \times \mathbf{B} - \nabla p_{\mathrm{e}})$

plus magnetostatics

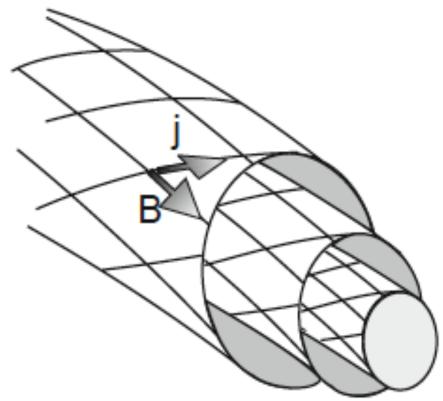


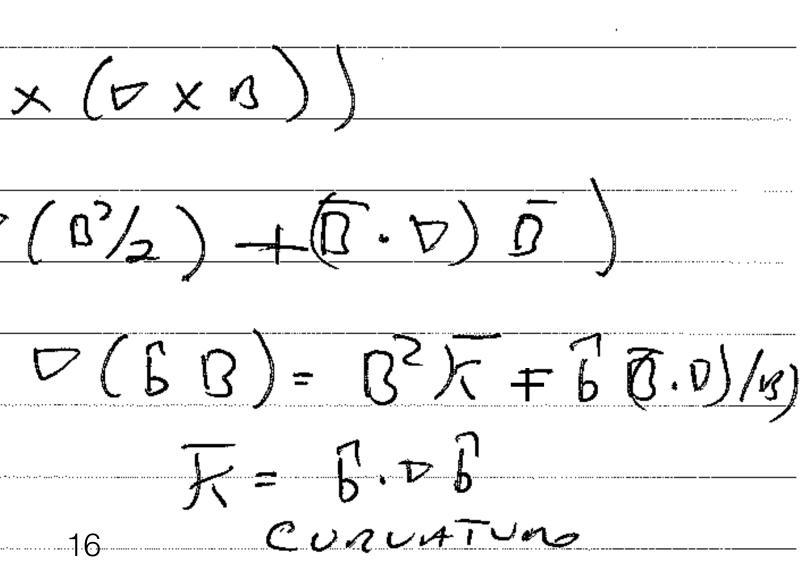
$\frac{\partial n}{\partial t} + \nabla \cdot (n\mathbf{u}) = 0$



$\nabla \times \mathbf{B} = \mu_0 \mathbf{j}$ $\mathbf{0} = \mathbf{j} \times \mathbf{B} - \nabla p$ (12) $\nabla (\mathbf{A} \cdot \mathbf{B}) = \mathbf{A} \times (\nabla \times \mathbf{B}) + \mathbf{B} \times (\nabla \times \mathbf{A}) + (\mathbf{A} \cdot \nabla)\mathbf{B} + (\mathbf{B} \cdot \nabla)\mathbf{A}$ $\nabla P = J \times \overline{D}$ $= \frac{1}{M_0} \left(-\overline{D} \times (\nabla \times N) \right)$ $= \frac{1}{m} \left(- \nabla \left(\frac{0}{2} \right) - \frac{1}{2} \left(\overline{0} \cdot \nabla \right) \overline{0} \right)$ B) = B2× = 6 (0.0)/3) · 5) g = 13. 0 (6 DUT

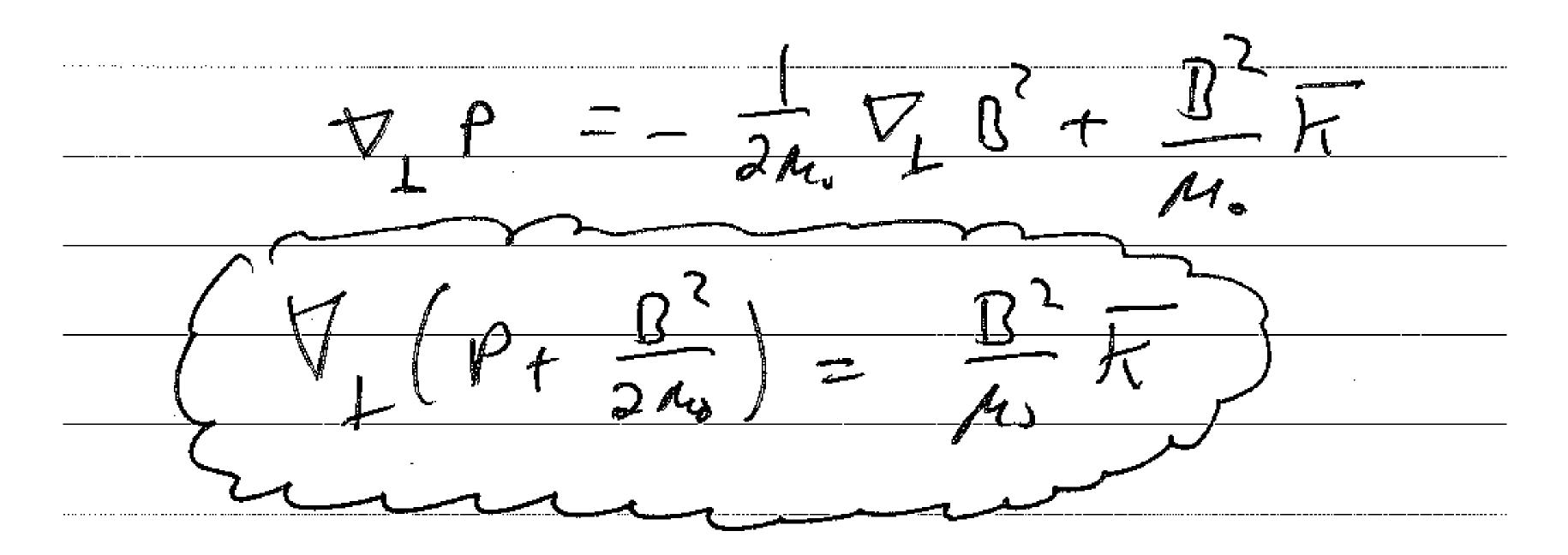
Statics



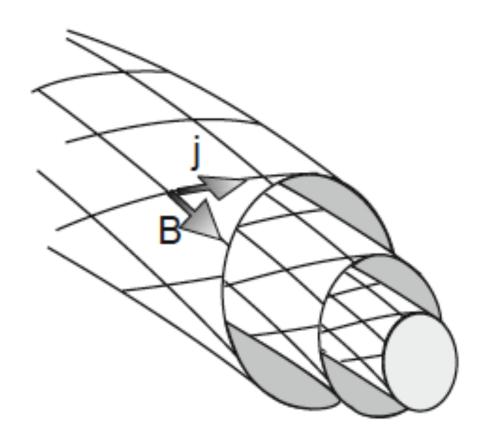


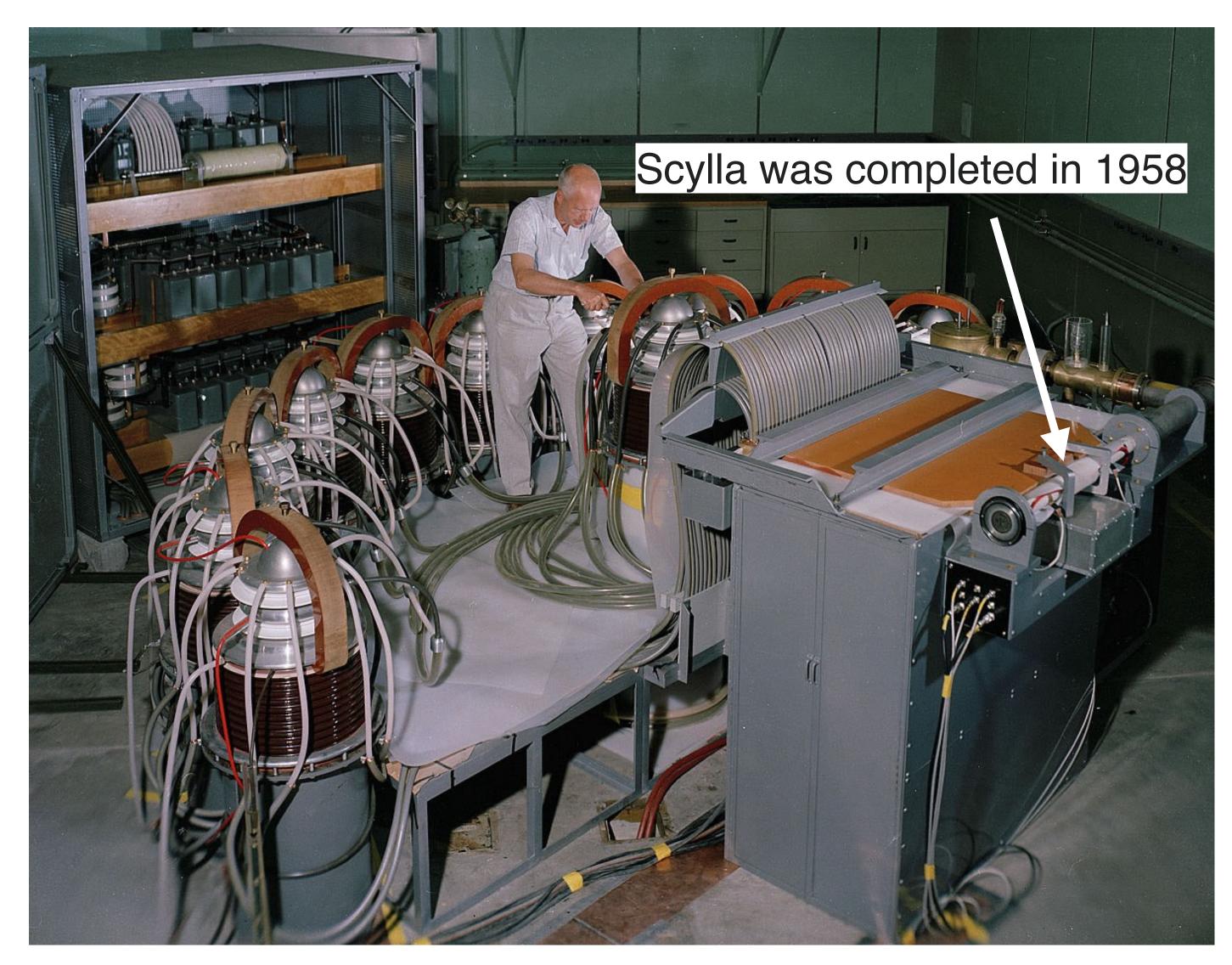


$\nabla \times \mathbf{B} = \mu_0 \mathbf{j}$ $\mathbf{0} = \mathbf{j} \times \mathbf{B} - \nabla p$

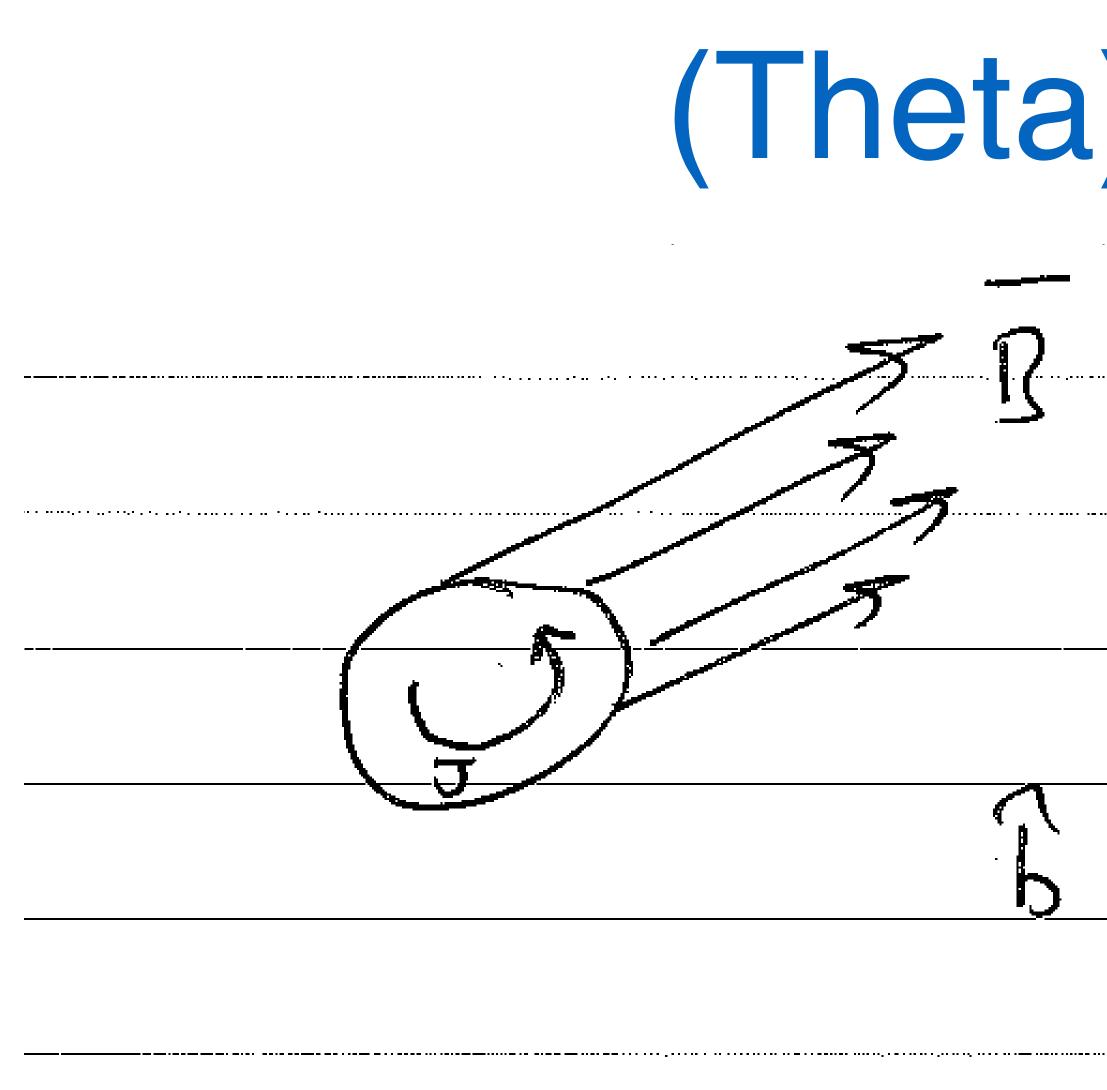


Statics





(Theta) θ-Pinch



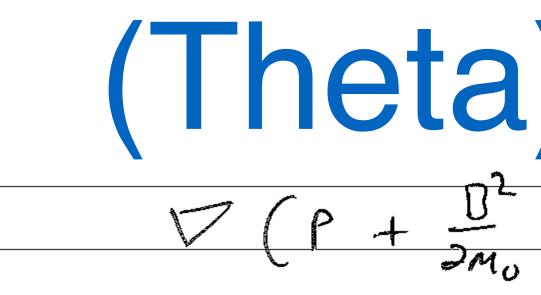
STRAIGHT B-LINES

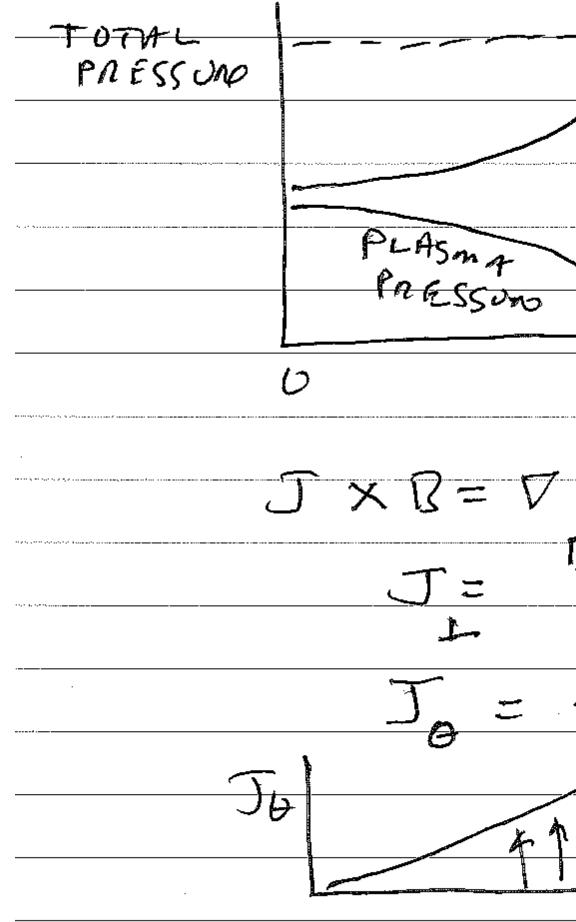
(Theta) θ-Pinch

= B(x) 2

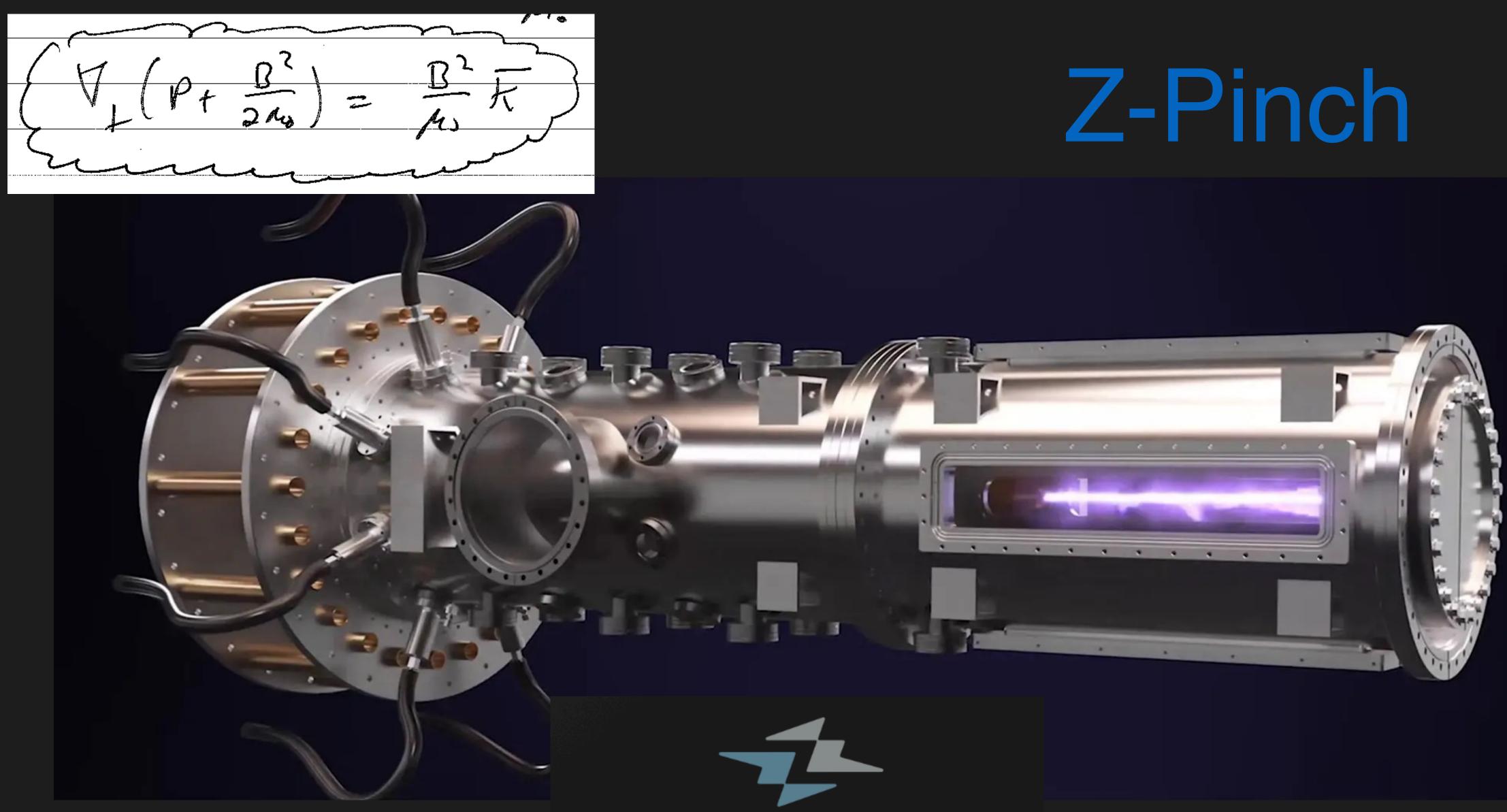
= 2. 22 0

NO CURVANDO



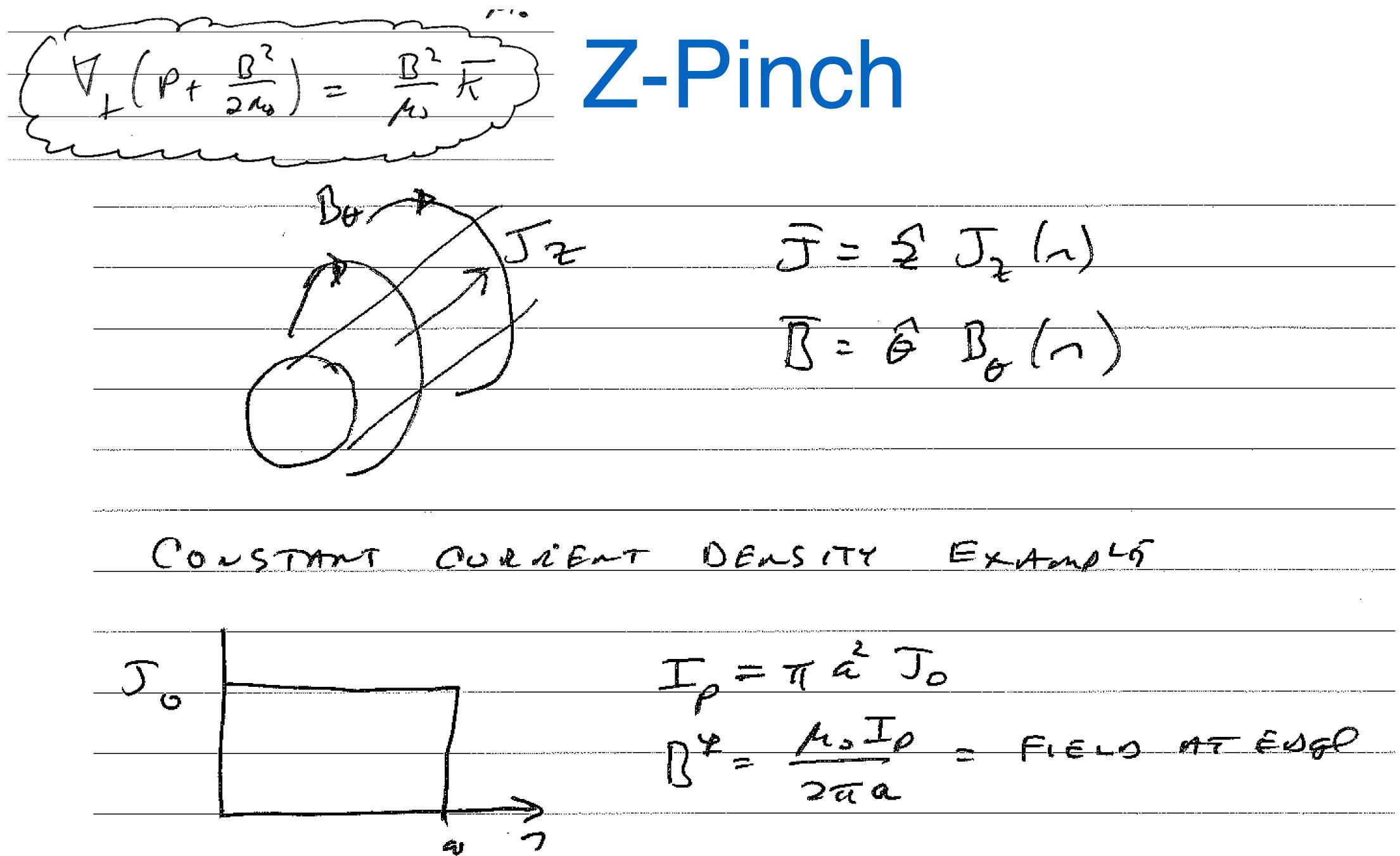


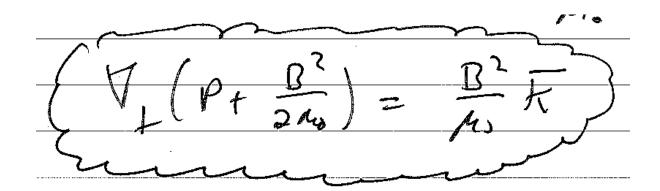
) 0-	-Pinch
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<i>و</i>	
	MAGNERL
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9	
P	
BZ BZ	= DIAMAGNETOC CURRENT
1 2p B Z	
C.	



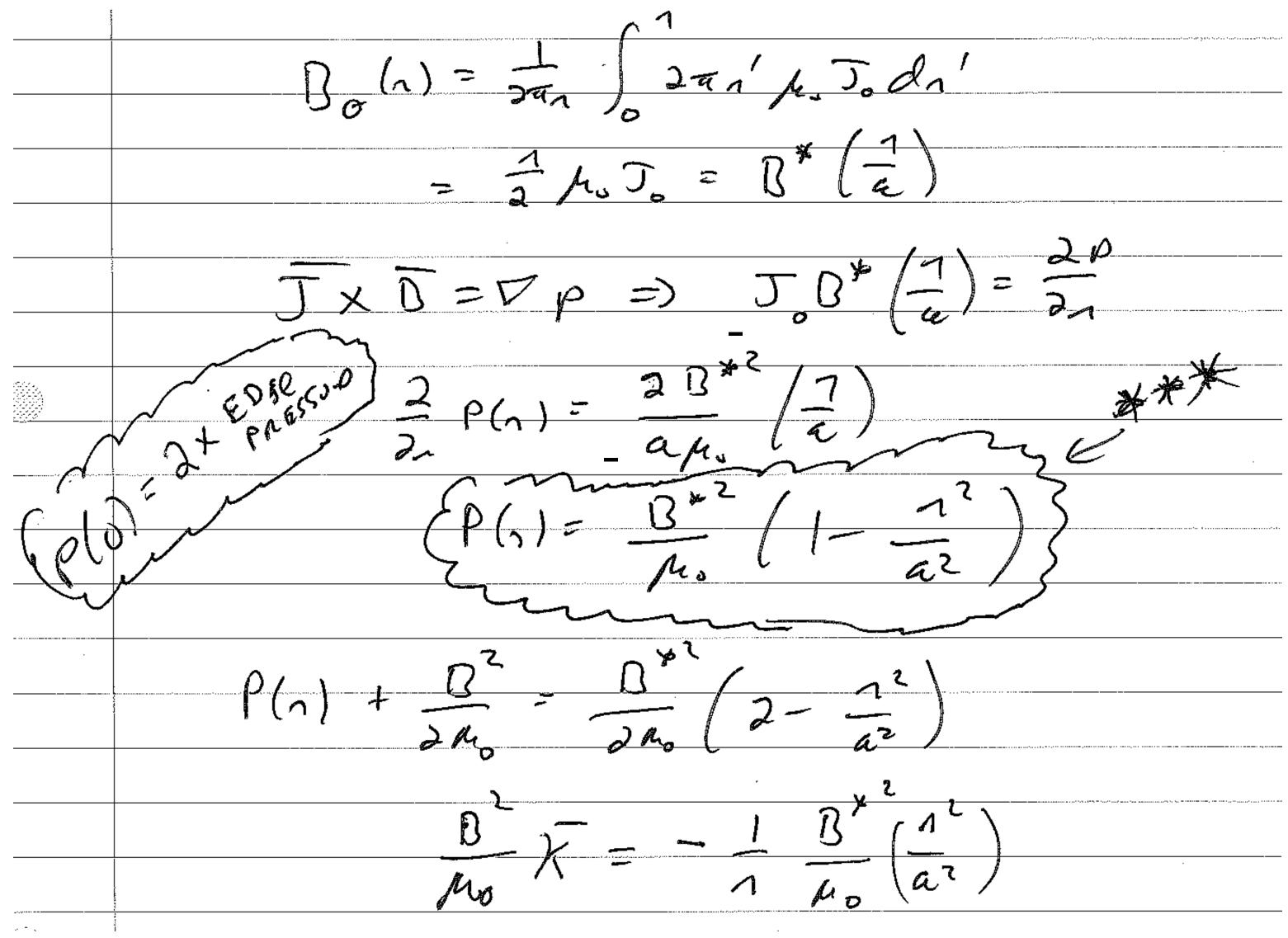
Fusion power. No magnets required.

ZAP ENERGY

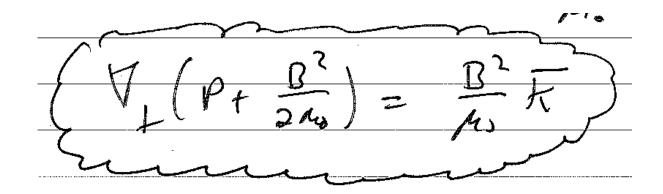




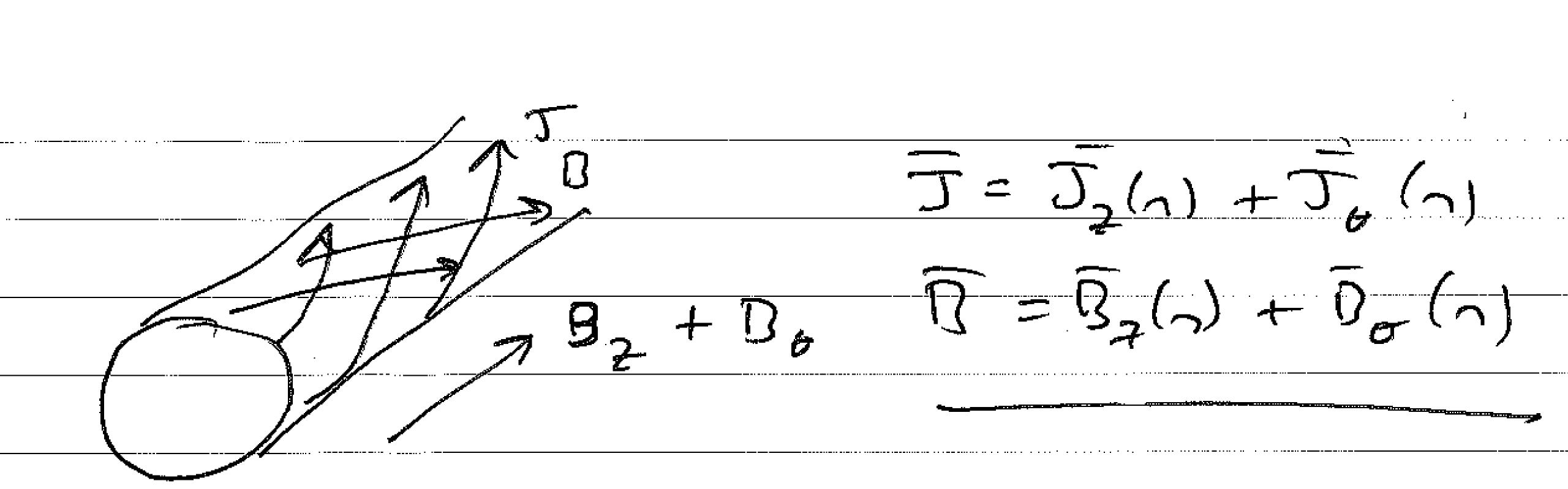


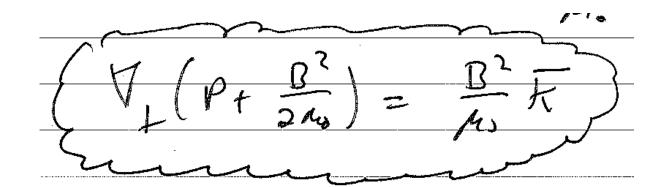


Z-Pinch

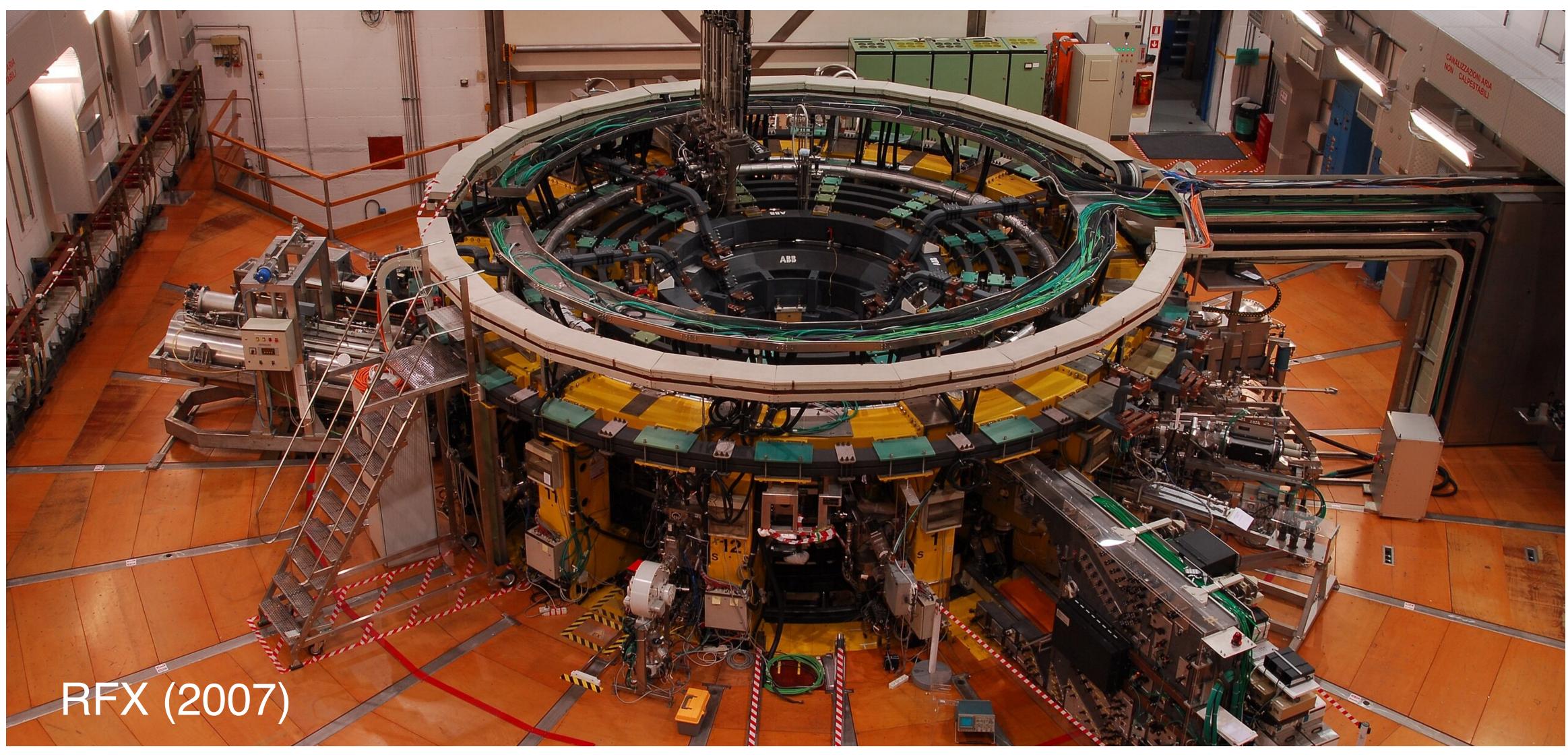


"Screw-Pinch" (a.k.a. "Straight Tokamak")

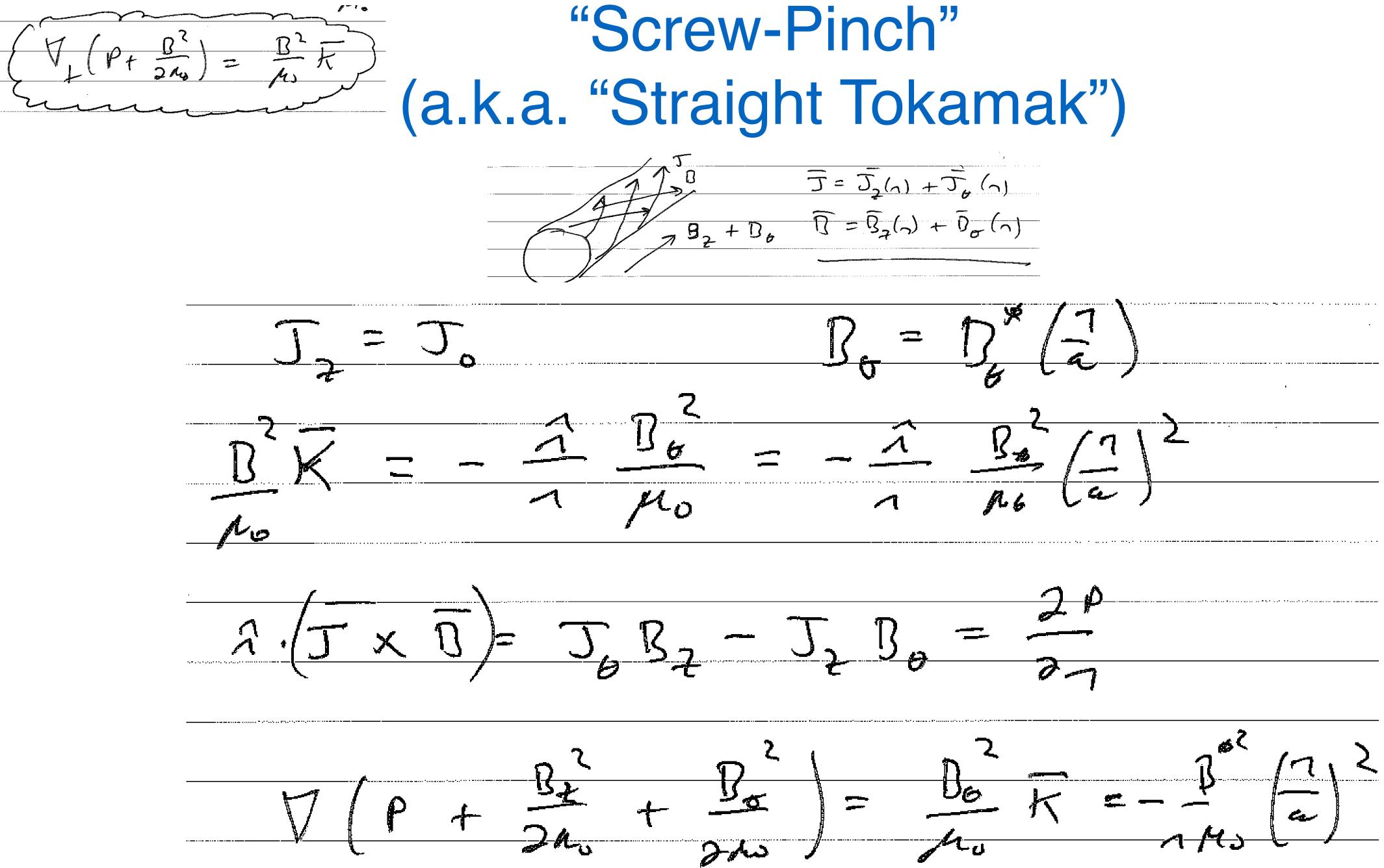








"Screw-Pinch" (a.k.a. "Straight Tokamak" or "Straight RFP")



"Screw-Pinch" (a.k.a. "Straight Tokamak"), LE $\overline{J} = \overline{J}_2(n) + \overline{J}_{\theta}(n)$ ß $\widehat{\Pi} = \widehat{B}_{2}(\gamma) + \widetilde{D}_{\sigma}(\gamma)$ 792+D0 2

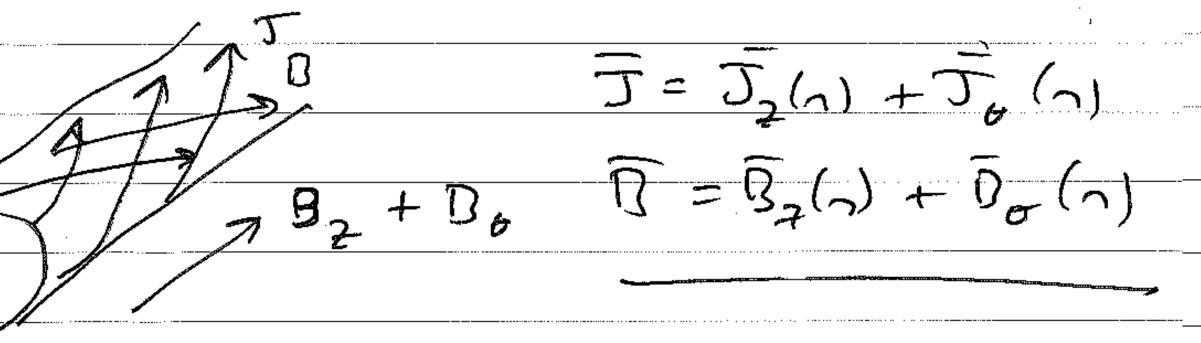
$$\nabla \left(P + \frac{B_{x}^{2}}{2A_{0}} + \frac{P_{x}^{2}}{2A_{0}} \right) = \frac{B_{0}^{2}}{A_{0}} \overline{K} = -\frac{P_{0}^{2}}{A_{0}} \left(\frac{P_{0}}{A_{0}} + \frac{P_{0}^{2}}{2A_{0}} \right)$$

$$\overline{P} \left(-\frac{P_{0}}{A_{0}} + \frac{P_{0}^{2}}{A_{0}} + \frac{(\Delta B_{2})^{2}}{2A_{0}} + \frac{(\Delta B_{2})^{2}}{2A_{0}} \right)^{2} \left(-\frac{P_{0}}{A_{0}} + \frac{(\Delta B_{2})^{2}}{2A_{0}} + \frac{P_{0}^{2}}{2A_{0}} \right) = -\frac{P_{0}^{2}}{A_{0}} \left(\frac{(\Lambda^{2})}{(\Delta P_{0})^{2}} \left(-\frac{P_{0}}{A_{0}} - \frac{(\Delta B_{2})^{2}}{2A_{0}} + \frac{P_{0}^{2}}{2A_{0}} \right) \right) = -\frac{P_{0}^{2}}{A_{0}} \left(\frac{(\Lambda^{2})}{(\Delta P_{0})^{2}} \left(-\frac{P_{0}}{A_{0}} - \frac{(\Delta B_{2})^{2}}{2A_{0}} + \frac{P_{0}^{2}}{2A_{0}} \right) \right) = -\frac{P_{0}^{2}}{A_{0}} \left(\frac{(\Lambda^{2})}{(\Delta P_{0})^{2}} \left(-\frac{P_{0}}{(\Delta P_{0})^{2}} + \frac{P_{0}^{2}}{2A_{0}} \right) \right) = -\frac{P_{0}^{2}}{A_{0}} \left(\frac{(\Lambda^{2})}{(\Delta P_{0})^{2}} \left(-\frac{(\Delta B_{2})^{2}}{(\Delta P_{0})^{2}} + \frac{P_{0}^{2}}{(\Delta P_{0})^{2}} \right) \right) = -\frac{P_{0}^{2}}{A_{0}} \left(\frac{(\Lambda^{2})}{(\Delta P_{0})^{2}} \left(-\frac{(\Delta B_{2})^{2}}{(\Delta P_{0})^{2}} + \frac{P_{0}^{2}}{(\Delta P_{0})^{2}} \right) \right) = -\frac{P_{0}^{2}}{(\Delta P_{0})^{2}} \left(\frac{(\Lambda^{2})}{(\Delta P_{0})^{2}} \left(-\frac{(\Lambda^{2})^{2}}{(\Delta P_{0})^{2}} + \frac{(\Lambda^{2})^{2}}{(\Delta P_{0})^{2}} \right) \right) = -\frac{P_{0}^{2}}{(\Delta P_{0})^{2}} \left(\frac{(\Lambda^{2})^{2}}{(\Delta P_{0})^{2}} \left(-\frac{(\Lambda^{2})^{2}}{(\Delta P_{0})^{2}} + \frac{(\Lambda^{2})^{2}}{(\Delta P_{0})^{2}} \right) \right) = -\frac{P_{0}^{2}}{(\Delta P_{0})^{2}} \left(\frac{(\Lambda^{2})^{2}}{(\Delta P_{0})^{2}} \left(-\frac{(\Lambda^{2})^{2}}{(\Delta P_{0})^{2}} + \frac{(\Lambda^{2})^{2}}{(\Delta P_{0})^{2}} \right) \right) = -\frac{P_{0}^{2}}{(\Delta P_{0})^{2}} \left(\frac{(\Lambda^{2})^{2}}{(\Delta P_{0})^{2}} + \frac{(\Lambda^{2})^{2}}{(\Delta P_{0})^{2}} \right) = -\frac{P_{0}^{2}}{(\Delta P_{0})^{2}} \left(\frac{(\Lambda^{2})^{2}}{(\Delta P_{0})^{2}} + \frac{(\Lambda^{2})^{2}}{(\Delta P_{0})^{2}} \right) = -\frac{P_{0}^{2}}{(\Delta P_{0})^{2}} \left(\frac{(\Lambda^{2})^{2}}{(\Delta P_{0})^{2}} + \frac{(\Lambda^{2})^{2}}{(\Delta P_{0})^{2}} \right) = -\frac{P_{0}^{2}}{(\Delta P_{0})^{2}} \left(\frac{(\Lambda^{2})^{2}}{(\Delta P_{0})^{2}} + \frac{(\Lambda^{2})^{2}}{(\Delta P_{0})^{2}} \right) = -\frac{P_{0}^{2}}{(\Delta P_{0})^{2}} \left(\frac{(\Lambda^{2})^{2}}{(\Delta P_{0})^{2}} + \frac{(\Lambda^{2})^{2}}{(\Delta P_{0})^{2}} \right) = -\frac{P_{0}^{2}}{(\Delta P_{0})^{2}} \left(\frac{(\Lambda^{2})^{2}}{(\Delta P_{0})^{2}} + \frac{(\Lambda^{2})^{2}}{(\Delta P_{0})^{2}} \right) = -\frac{P_{0}^{2}}{(\Delta P_{0})^{2}} \left(\frac{(\Lambda^{2})^{2}}{(\Delta P_{0})^{2}} + \frac{(\Lambda^{2})^{2}}{(\Delta P_{0})^{2}}$$

$$\frac{2\left(\pm P_{o}\pm\frac{(\Delta B_{+})^{2}}{2m_{o}}\pm\frac{B_{o}}{2m_{o}}\right)^{2}}{2m_{o}}=\frac{B_{o}}{m_{o}}$$



"Screw-Pinch" (a.k.a. "Straight Tokamak")



$$\frac{\left(P_{o} + \frac{\left(\Delta B_{7}\right)^{2}}{2\mu_{o}} - \frac{B_{o}}{2\mu_{o}}\right) = \frac{B_{o}}{\mu_{o}}}{B_{o}}$$

$$\frac{\beta_{\rho} + M - 1 = 0}{B_{\rho} + M - 1 = 0}$$

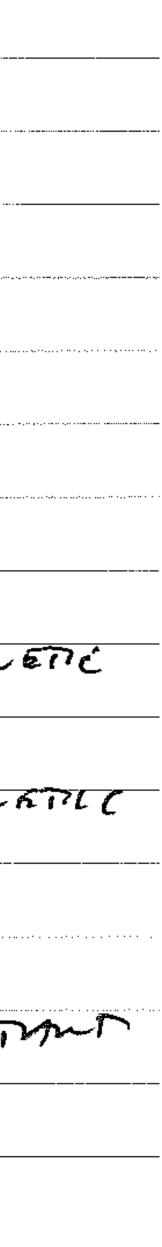
$$\frac{\beta_{\rho} = \frac{P_{o}}{B_{o} + M_{o}}}{B_{o} + M_{o}}$$

$$\frac{\beta_{\rho} = \frac{P_{o}}{B_{o} + M_{o}}}{B_{o} + M_{o}}$$

$$\frac{\beta_{\rho} = \frac{\left(\Delta B_{7}\right)^{2}}{B_{o} + M_{o}}}{C + D_{1} + M_{o}}$$

$$\frac{\beta_{\rho} = 1}{B_{\rho}} = \frac{\Delta B_{7}}{D_{1}} = 0$$

$$B_{7} = c_{o} + S_{1}$$



PLASMA EQUILIBRIUM IN A TOKAMAK

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ABSTRACT. The paper summarizes the basic information on the equilibrium of a toroidal plasma column in systems of the Tokamak type. It considers the methods of maintaining a plasma in equilibrium with the help of a conducting casing, an external maintaining field and the iron core of a transformer. Attention is paid to the role of the inhomogeneity of the maintaining field. It is shown in particular how the shape of the column cross-section depends on the curvature of the lines of force of the maintaining field. For the case (which has practical importance) weak asymmetry of the field distribution in the transverse cross-section, this paper describes a uniform method of consideration, which takes into account the influence of different factors on the equilibrium position of the column. This method is used for calculating plasma equilibrium in a Tokamak model with a conducting casing. Account is here taken of the effect of gaps in the casing and of finite electrical conductivity. Some cases of plasma equilibrium which are outside the standard Tokamak scheme are also considered, such as equilibrium in a conducting shell having the shape of a racetrack, equilibrium where the whole current is transferred by relativistic runaway electrons and equilibrium at high plasma pressure $\beta_{\rm I} \sim R/a$.

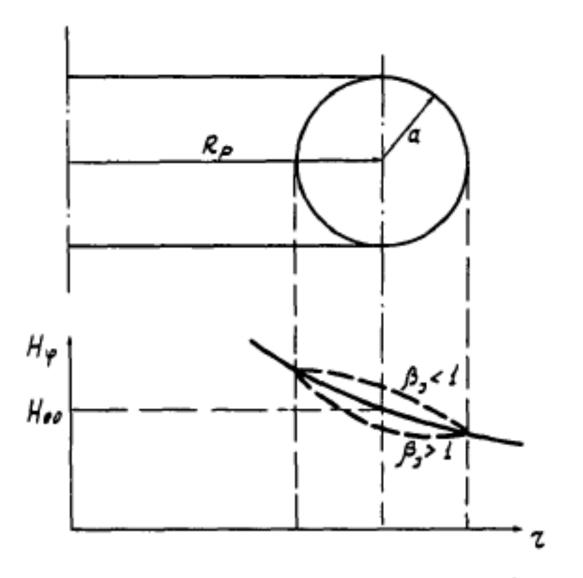


FIG.1. Distribution of a toroidal magnetic field.

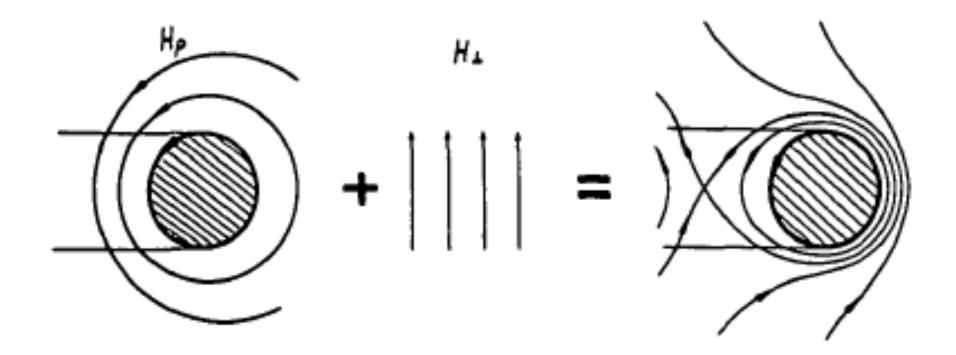


FIG.4. Diagram of the combination of the proper magnetic field of a ring current with transverse balancing magnetic field.

Numerical Determination of Axisymmetric Toroidal Magnetohydrodynamic Equilibria

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Numerical schemes for the determination of stationary axisymmetric toroidal equilibria appropriate for modeling real experimental devices are given. Iterative schemes are used to solve the elliptic nonlinear partial differential equation for the poloidal flux function Ψ . The principal emphasis is on solving the free boundary (plasma-vacuum interface) equilibrium problem where external current-carrying toroidal coils support the plasma column, but fixed boundary (e.g., conducting shell) cases are also included. The toroidal current distribution is given by specifying the pressure and either the poloidal current or the safety factor profiles as functions of Ψ . Examples of the application of the codes to tokamak design at PPPL are given.

Solution Procedure with $p(\Psi)$ and $g(\Psi)$ Specified

$$abla p = \mathbf{J} \times \mathbf{B},$$
 $\mathbf{J} = \mathbf{\nabla} \times \mathbf{B},$
 $\mathbf{B} = \frac{1}{2\pi} \, \mathbf{\nabla} \phi \, \times \, \mathbf{\nabla} \phi$
 $\mathbf{\nabla} \cdot \mathbf{B} = 0.$

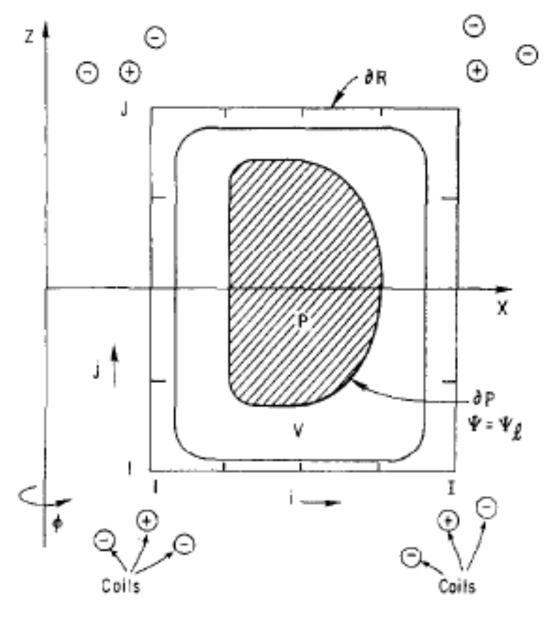


FIG. 1. Computational domain R.

$$X \frac{\partial}{\partial X} \frac{1}{X} \frac{\partial \Psi}{\partial X} + \frac{\partial^2 \Psi}{\partial Z^2} = 2\pi X J_{\phi},$$

 $\Psi + RB_0g \nabla \phi$

$$J_{\phi} = -2\pi \left(X \frac{dp}{d\Psi} + \frac{R^2 B_0^2}{2X} \frac{dg^2}{d\Psi} \right).$$

Grad-Shafranov Equation

 $\nabla \times \mathbf{B} = \mu_0 \mathbf{j}$

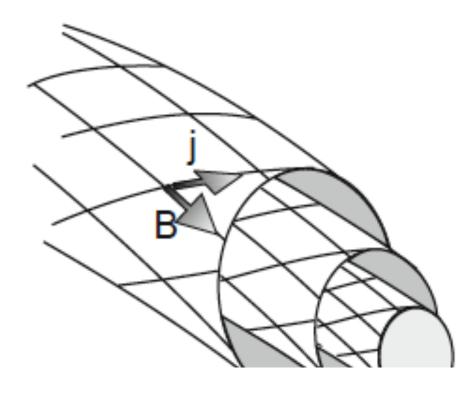
 $\mathbf{0} = \mathbf{j} \times \mathbf{B} - \nabla p$

• $\overline{R} = \overline{\nabla} \rho \times \overline{\nabla} \gamma + G \overline{\nabla} \gamma$

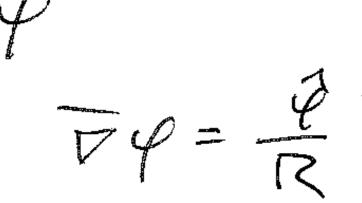
CYLINDRICAL SYMMETRY $\overline{\nabla \varphi} = \frac{1}{\overline{R}}$

6 = TOROIDAL FLUX BOS = GA • P(4), 6(4)

 $\overline{B} \cdot \overline{B} = (\nabla \varphi \times \nabla \psi) \cdot (\nabla \psi)$ $= |\nabla \varphi|^{2} (|\nabla \Psi|^{2})$





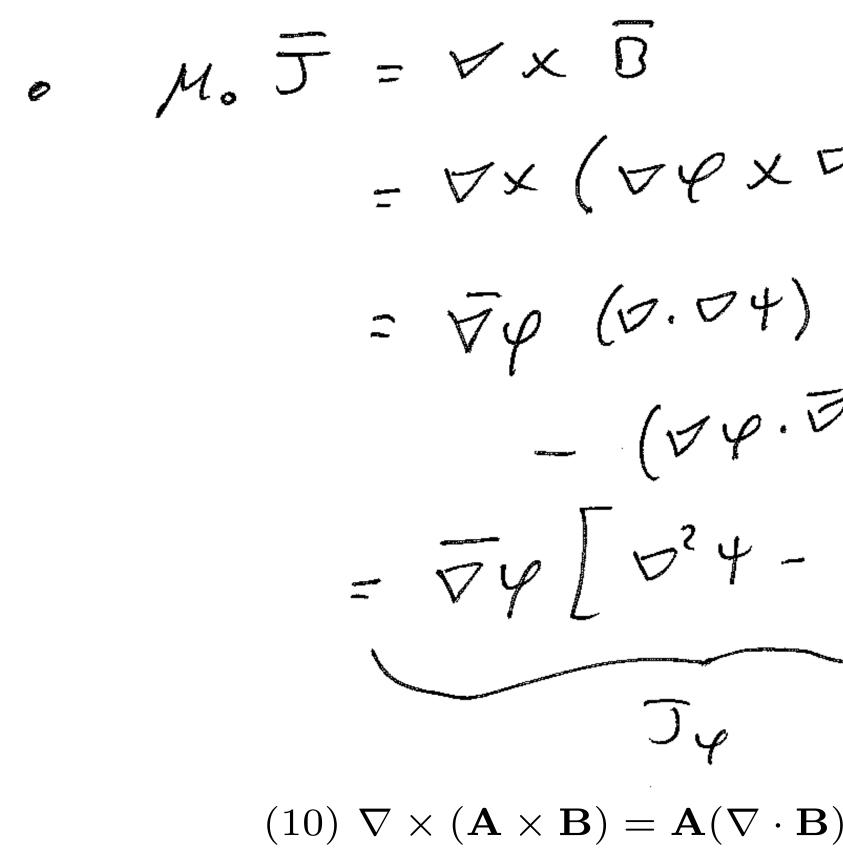


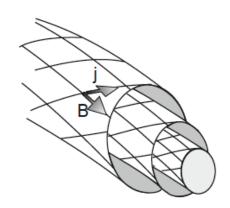
TY. F(ANTTHINT)=0

$$\varphi \times \varphi + 6^2 (\varphi + 6^2)^2$$

Grad-Shafranov Equation

- $\nabla \times \mathbf{B} = \mu_0 \mathbf{j}$
- $0 = \mathbf{j} \times \mathbf{B} \nabla p$



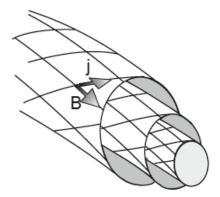


 $= \nabla \times (\nabla \varphi \times \nabla \Psi) + \nabla \times (6 \nabla \varphi)$ $= \overline{\nabla}\varphi \ (\overline{\upsilon}.\overline{\upsilon}+) - \overline{\upsilon}+ (\overline{\upsilon}.\overline{\upsilon}\varphi) + (\overline{\upsilon}+.\overline{\upsilon})\overline{\upsilon}\varphi \\ - (\overline{\upsilon}\varphi.\overline{\upsilon})\overline{\upsilon}+ + 6 \ \overline{\upsilon}\times\overline{\upsilon}\varphi + \overline{\upsilon}6 \ \overline{\varkappa}\overline{\upsilon}\varphi$ $= \overline{\nabla Y} \left[\overline{\nabla^2 Y} - \frac{1}{2\pi} \frac{2Y}{2\pi} \right] + \frac{26}{24} \overline{\nabla Y} \times \overline{\nabla Y} \right]$

(10) $\nabla \times (\mathbf{A} \times \mathbf{B}) = \mathbf{A}(\nabla \cdot \mathbf{B}) - \mathbf{B}(\nabla \cdot \mathbf{A}) + (\mathbf{B} \cdot \nabla)\mathbf{A} - (\mathbf{A} \cdot \nabla)\mathbf{B}$ 32

Grad-

$$\nabla \times \mathbf{B} = \mu_0 \mathbf{j}$$
$$0 = \mathbf{j} \times \mathbf{B} - \nabla p$$



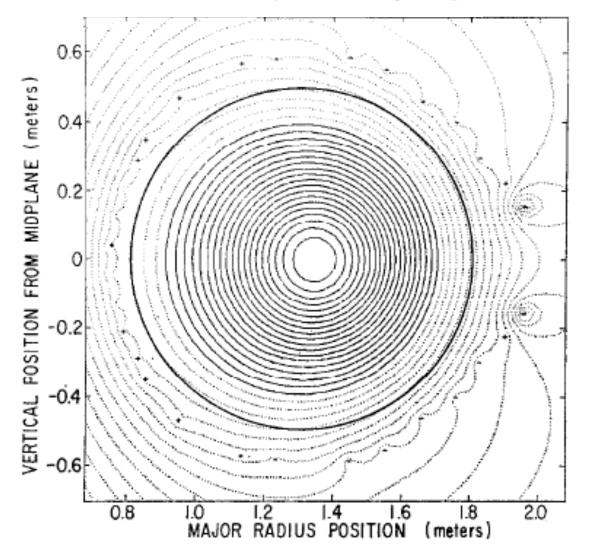
-Shafranov Equation

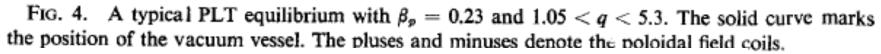
$$\begin{aligned}
\overline{\nabla}r &= \overline{\mathcal{T}} \times \overline{\mathcal{G}} \\
\mathcal{M}_{o} \overline{\nabla} \psi \cdot \overline{\nabla} \rho &= \overline{\nabla} \psi \quad \mu_{o} \cdot (\overline{\mathcal{T}} \times \overline{\mathcal{B}}) \\
\mathcal{M}_{o} | \overline{\nabla} \psi |^{2} \frac{2\rho}{2\psi} &= \mathcal{M}_{o} \cdot \overline{\mathcal{T}} \cdot (\overline{\mathcal{R}} \times \overline{\nabla} \psi) \\
&= \mathcal{M}_{o} \cdot \overline{\mathcal{T}} \cdot \left[-\overline{\nabla} \psi \times (\overline{\nabla} \rho \times \nabla \psi) \\
&= \mathcal{M}_{o} \cdot \overline{\mathcal{T}} \cdot \left[-\overline{\nabla} \psi \times (\overline{\nabla} \rho \times \nabla \psi) \\
&= -\mathcal{M}_{o} \cdot \overline{\mathcal{T}} \rho | \overline{\nabla} \psi | | \overline{\nabla} \psi |^{2} + \mathcal{H}_{o} \cdot (\overline{\mathcal{T}} \cdot \nabla \rho \times \nabla \psi) \\
&= -\mathcal{M}_{o} \cdot \overline{\mathcal{T}} \rho | \overline{\nabla} \psi | | \overline{\nabla} \psi |^{2} + \mathcal{G} \cdot \frac{2^{2}}{2\psi} (\overline{\nabla} \phi \times \nabla \phi) \cdot (\overline{\nabla} \phi \times \nabla \psi) \\
&= -\mathcal{M}_{o} \cdot \overline{\mathcal{T}} \rho | \overline{\nabla} \psi | | \overline{\nabla} \psi |^{2} - \frac{2^{2}}{2\psi} (\overline{\nabla} \phi \times \nabla \phi) \cdot (\overline{\nabla} \phi \times \nabla \phi) \\
&= -\mathcal{M}_{o} \cdot \overline{\mathcal{T}} \rho | \overline{\nabla} \psi | | \overline{\nabla} \psi |^{2} - \frac{2^{2}}{2\psi} (\overline{\nabla} \phi \times \nabla \phi) \cdot (\overline{\nabla} \phi \times \nabla \phi) \\
&= -\mathcal{M}_{o} \cdot \overline{\mathcal{T}} \rho | \overline{\nabla} \psi |^{2} - \frac{2^{2}}{2\psi} - \frac{2^{2}}{6 \cdot 2\psi} (\overline{\nabla} \phi - \overline{\mathcal{T}} \theta) \\
&= -\mathcal{M}_{o} \cdot \overline{\mathcal{T}} \rho | \overline{\nabla} \psi |^{2} - \frac{2^{2}}{2\psi} - \frac{2^{2}}{6 \cdot 2\psi} (\overline{\nabla} \phi - \overline{\mathcal{T}} \theta) \\
&= -\mathcal{M}_{o} \cdot \overline{\mathcal{T}} \rho | \overline{\nabla} \psi |^{2} + \frac{2^{2}}{2\psi} - \frac{2^{2}}{6 \cdot 2\psi} (\overline{\nabla} \phi - \overline{\mathcal{T}} \theta) \\
&= -\mathcal{M}_{o} \cdot \overline{\mathcal{T}} \rho | \overline{\nabla} \psi |^{2} + \frac{2^{2}}{2\psi} - \frac{2^{2}}{2\psi} \partial \psi |^{2} + \frac{2^{2}}{2\psi} \partial \psi |^{$$

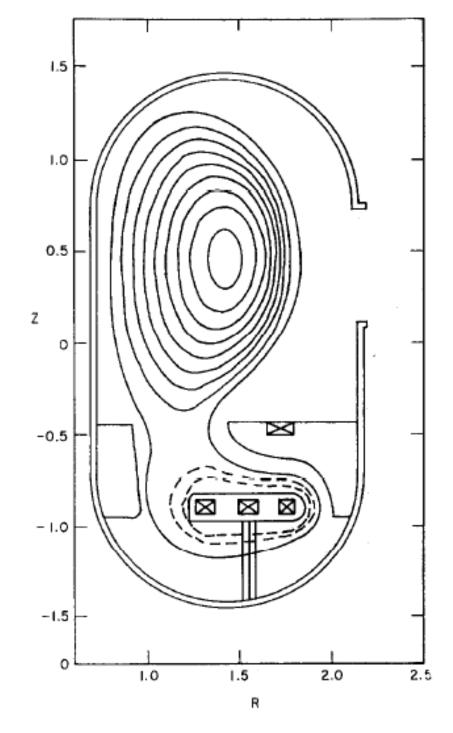


(1) $\mathbf{A} \cdot \mathbf{B} \times \mathbf{C} = \mathbf{A} \times \mathbf{B} \cdot \mathbf{C} = \mathbf{B} \cdot \mathbf{C} \times \mathbf{A} = \mathbf{B} \times \mathbf{C}$ (2) $\mathbf{A} \times (\mathbf{B} \times \mathbf{C}) = (\mathbf{C} \times \mathbf{B}) \times \mathbf{A} = (\mathbf{A} \cdot \mathbf{C})\mathbf{B} - (\mathbf{A} \cdot \mathbf{B})\mathbf{C}$

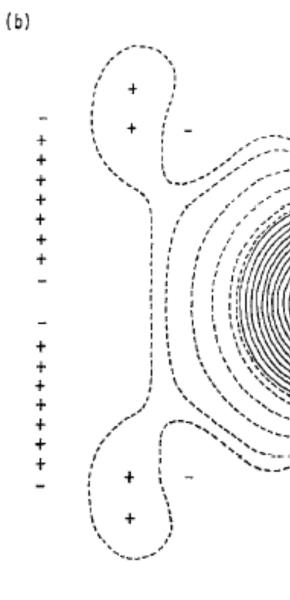
JOURNAL OF COMPUTATIONAL PHYSICS 32, 212-234 (1979)







(a)



IG. 6. Typical PDX equilibria, showing that the plasma can be attac s or (b) the outside divertor coils. Here $\alpha = \beta = 2$.

April 1989

make it come true. The ny's HyperAnimator lets nt or scan in faces and pe whatever you want o say; the text is automatonverted to speech syned with the lip move-Mom's voice won't like hers, however, una can get her to digitize ive you the disk. If you type in her words, she'll distinctly computerish. If n't have time to draw or ces, you can use the staine characters provided tStar

erAnimator's best adnan, however, is probaert, a talking head star-Disney's new version of bsent-Minded Professor," n Sunday nights as part World of Disney" TV seftware developers Jay n and Harry Anderson Albert to play the proelectronic sidekick. ntStar has also added the inimator's audio feature mail package called Mail, which lets your anicoworkers deliver their es in persona. erAnimator lists for . For further informantact BrightStar Techin Bellevue, Washing-206/885-5446. Farrison

aMack

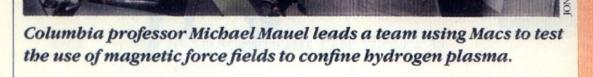
The U.S. Department

looks like rings of lightning and lasts for 200 millionths of a second each time it appears. During every flash of the lightning ring, laser beams and magnetic sensors measure the dynamics of the ring at least once every millionth of a second, producing more than a megabyte of data.

The data is digitized, loaded into VAX computers, transferred to Macs, and then analyzed with TokaMack, an application Mauel wrote using Apple's Macintosh Programmer's Workshop (MPW) and MacApp. The analysis also involves four Cray comtohydrodynamic instabilities, called kinks, occurring in the plasma ring at very high pressure.

TokaMack is named after Tokamak, an earlier device developed by the late Russian physicist L. A. Artsimovich for magnetically confining ring lightning. Mauel offers the software as freeware to scientists doing similar research throughout the world. TokaMack requires a Mac II.

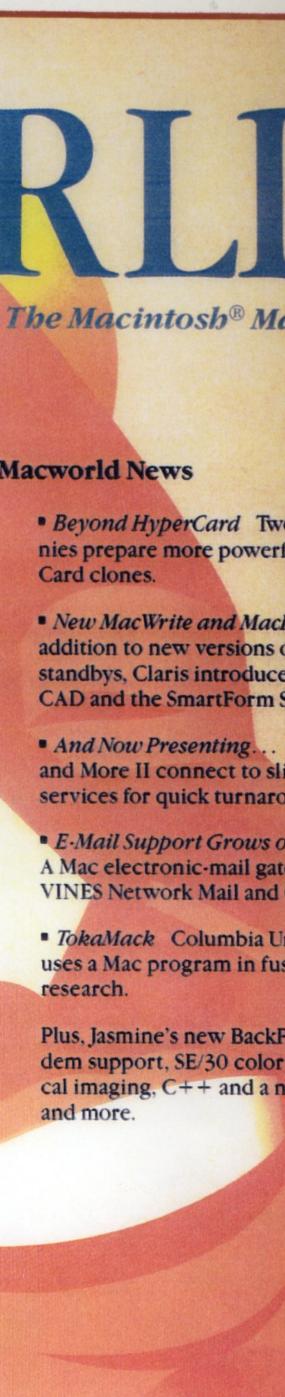
For further information, contact Michael Mauel at Columbia University, at 212/854-4455. -Ann Garrison



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- Card clones.

- research.
- and more.





- More Piel / Chapter 5: "Fluid" Equations
- "Frozen-in" flux condition
- Alfvén wave
- Monday, October 9: Homework #5

Next Lecture