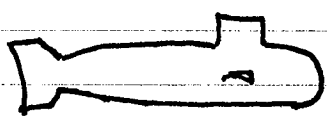


APPH 4200 HW5 : SOLUTIONS

#1 PROBLEM 8.2



1/25<sup>TH</sup> SCALE  
MODEL

WIND TUNNEL TEST: P = 200 kPa  
(~ 2 ATM)  
T = 300°K  
(~ 27° C)

WHAT VELOCITY TO BE SIMILAR  
TO 30 km/hr AT FULL SCALE?

SINCE MODEL/SUB IS FAR FROM SURFACE, THEY  
ARE SIMILAR WHEN HAVING EQUAL REYNOLDS  
NUMBERS. THIS MEANS THE DRAG (VISCOUS)  
COEFFICIENTS WILL BE EQUAL.

$$Re = \frac{UL}{\nu} \Big|_{\text{MODEL}} = \frac{UL}{\nu} \Big|_{\text{FULL}}$$

$$U_{\text{MODEL}} = U_{\text{FULL}} \left( \frac{L_{\text{FULL}}}{L_{\text{MODEL}}} \right) \left( \frac{\nu_{\text{MODEL}}}{\nu_{\text{FULL}}} \right)$$

↑  
30 km/hr      ↑  
25

$$\frac{\nu_{\text{AIR}}}{\nu_{\text{WATER}}} = \frac{1.6 \times 10^{-5}}{1.0 \times 10^{-6}} \approx 16$$

SO  $U_{\text{MODEL}} = U_{\text{FULL}} \times 400$

BUT SPEED OF SOUND IS 1.5 km/s  
OR 5,400 km/hr. THUS, MODEL SPEED MUST  
BE FASTER THAN SPEED OF SOUND! THIS MAKES  
THE MODEL TEST INVALID SINCE THE MACH  
NUMBER WILL NOT BE THE SAME IN BOTH CASES

$$\text{COEFFICIENT OF DRAG} = \frac{D_o}{\rho U^2 L} \Big|_{\text{MODEL}} = \frac{D}{\rho U^2 L} \Big|_{\text{FULL}}$$

#1 CONTINUED

THUS 
$$\frac{D_{\text{MODEL}}}{D_{\text{FULL}}} = \left( \frac{\rho_{\text{MODEL}}}{\rho_{\text{FULL}}} \right) \left( \frac{U_m}{U_{\text{FULL}}} \right)^2 \left( \frac{L_{\text{MODEL}}}{L_{\text{FULL}}} \right)^2$$

$= 0.522$

WHERE  $\rho_{\text{MODEL}} = (\rho/RT)_{\text{MODEL}} = 2.32 \text{ kg/m}^3$

$\rho_{\text{WATER}} = 1000 \text{ kg/m}^3$

#2 PROBLEM: NON-DIMENSIONALIZE HEAT CONDUCTION EQ

$$\frac{\partial T}{\partial t} = \frac{\partial T}{\partial t} + (u \cdot \nabla) T = K \nabla^2 T$$

NOTE: SINCE THIS EQUATION IS LINEAR IN T, T IS MADE NON-DIMENSIONAL TRIVIAALLY.

LET  $\nabla^2 \rightarrow \frac{1}{L^2} \nabla'^2$        $u \rightarrow u_0 u'$

time  $\rightarrow t/t_0$        $\frac{\partial}{\partial t} \rightarrow \frac{u_0}{L} \frac{\partial}{\partial t'}$

THEN, 
$$\frac{u_0}{L} \left( \frac{\partial T}{\partial t'} + u' \cdot \nabla' T \right) = \frac{K}{L^2} \nabla'^2 T$$

OR 
$$\frac{\partial T}{\partial t'} + u' \cdot \nabla' T = \frac{K}{u_0 L} \nabla'^2 T$$

$P_E = \text{PECLET NUM}$   $\uparrow$

$$P_E = \frac{uL}{K} = \text{RATIO OF THERMAL ADVECTION TO THERMAL DIFFUSION}$$

### #3: PROBLEM: HOW DOES VISCOSITY DAMP DEEP WATER GRAVITY WAVES?

REVIEW: THE SURFACE IS MOVING VERTICALLY AS

$$\eta(x,t) = \eta_0 \cos(kx - \omega t)$$

IF WE ASSUME  $\nabla \times \bar{u} = 0$  THEN  $\bar{u} = \nabla \psi$  (VELOCITY POTENTIAL). SINCE  $\nabla \cdot \bar{u} = 0$ , THEN  $\nabla^2 \psi = 0$ .

AT THE SURFACE, WE REQUIRE  $\frac{\partial \eta}{\partial t} \approx \frac{\partial \psi}{\partial z}$  AT  $z = \eta \approx 0$

AND ALSO BERNOULLI:  $\frac{\partial \psi}{\partial t} + g\eta \approx 0$

THIS SOLUTION IS  $\omega^2 = kg$  WITH  $\psi(x,z,t) = \psi_0 e^{kz} \sin(kx - \omega t)$   
WITH  $\psi_0 = \eta_0 \left(\frac{\omega}{k}\right)$  FOR  $z < 0$

NOTICE AT THE SURFACE  $u_x \approx \frac{\partial \psi}{\partial x} \approx \psi_0 k \cos(kx - \omega t)$

AT ANY POINT AT THE SURFACE, THE FLOW OSCILLATES BACK-N-FORTH TANGENTIALLY. THIS WILL GENERATE VISCOUS PERTURBATIONS NEAR THIS SURFACE. BERNOULLI'S PRINCIPLE CAN NOT BE APPLIED IN THIS THIN BOUNDARY. (SEE CLASS NOTES FOR NOV 20, 2007.)

AWAY  
HOWEVER, FAR FROM THE SURFACE; THE FLOW WILL BE IRROTATIONAL, AND  $\bar{u} = \nabla \psi$ . SUBSTITUTING THIS INTO NAVIER-STOKES...

$$\frac{\partial \bar{u}}{\partial t} = -g\hat{z} + \nu \nabla^2 \bar{u} \Rightarrow \nabla \left( \frac{\partial \psi}{\partial t} + gz - \nu \nabla^2 \psi \right) = 0$$

BUT  $\nabla^2 \psi = 0$ , SO VISCOSITY HAS NO INFLUENCE ON THE FLOW WHEN  $\nabla \times \bar{u} = 0$ .

#3 CONTINUED

HOW TO ESTIMATE VISCOUS DAMPING FOR WEAK VISCOSITY?

WAVE ENERGY = (MECHANICAL ENERGY OF OSCILLATIONS) + (POTENTIAL ENERGY OF OSCILLATIONS)

RATE OF VISCOUS DISSIPATION = -2μ ∑ Eij^2

Eij -> Exz = Ezx = 1/2 (2ux/z + 2uz/x) = z^2 φ / (2x2z) = -φ0 k^2 sin(kx - ωt) Q

WE KNOW THAT POTENTIAL AND KINETIC ENERGIES ARE EQUAL, SO

WAVE ENERGY = 2 (1/2 ρ U^2) = ρ [(2φ/x)^2 + (2φ/z)^2] = ρ k^2 φ0^2 e 2kz

WAVE (AMPLITUDE) DAMPING RATE = γ = -1/2 (VISCOUS DISSIPATION) / (WAVE ENERGY)

WHERE WE MUST TIME AVERAGE THE VISCOUS DISSIPATION. THEREFORE:

γ = 1/2 (2μ 2φ0^2 k^4 sin^2) / (ρ k^2 φ0^2) = 2k^2 ν. NOTE: γ/ω ~ k^2 (2ν / sqrt(kg))

VISCOUS BOUNDARY LAYER << 1

PROBLEM #3 (AGAIN)

(1)



$$\bar{u} = \nabla \psi \quad \psi(x, z, t) = \text{Re} \left\{ \phi e^{-i(\omega t - kx)} e^{kz} \right\}$$

For  $z < 0$

$$\begin{aligned} \text{WAVE ENERGY} &= \iiint dV \left( \frac{1}{2} \rho u^2 + \rho g(z - \bar{z}) \right) \\ &= 2 \times \iiint dV \frac{1}{2} \rho u^2 \end{aligned}$$

$$\begin{aligned} u^2 &\propto \bar{u}^* \cdot \bar{u} = \frac{2\phi^*}{2x} \cdot \frac{2\phi}{2x} + \frac{2\phi^*}{2z} \cdot \frac{2\phi}{2z} \\ &= |\phi|^2 k^2 e^{2kz} + |\phi|^2 k^2 e^{2kz} \end{aligned}$$

$$\begin{aligned} \text{DISSIPATION} &= \iiint dV 2\mu \epsilon_{ij}^2 \\ &= \iiint dV 2\mu \epsilon_{ij}^* \epsilon_{ij} \end{aligned}$$

$$\epsilon_{ij} = \left\{ \epsilon_{xx}, \epsilon_{zz}, \epsilon_{xz}, \epsilon_{zx} = \epsilon_{xz} \right\}$$

$$\epsilon_{xx} = \frac{2u_x}{2x} = \frac{2^2 \phi}{2x^2} = -k^2 \phi$$

$$\epsilon_{zz} = \frac{2u_z}{2z} = \frac{2^2 \phi}{2z^2} = -k^2 \phi$$

$$\epsilon_{xz} = \frac{1}{2} \left( \frac{2u_x}{2z} + \frac{2u_z}{2x} \right) = \frac{2^2 \phi}{2x2z} = ik^2 \phi$$

$$\begin{aligned} \epsilon_{ij}^* \epsilon_{ij} &= k^4 |\phi|^2 + k^4 |\phi|^2 + 2k^4 |\phi|^2 \\ &= 4k^4 |\phi|^2 \end{aligned}$$

$$\frac{d}{dt} (\text{WAVE ENERGY}) = - 2\gamma (\text{WAVE ENERGY})$$

$$= - (\text{DISSIPATION})$$

$$\therefore \gamma \equiv \frac{\text{DISSIPATION}}{2 (\text{WAVE ENERGY})}$$

$$\propto \frac{8 \nu \rho h^4 |\psi|^2}{4 \rho h^2 |\psi|^2}$$

$$\gamma = 2 \nu h^2$$

THEIR FORM

$$\psi(x, z, t) = R \left\{ \psi e^{-i(\omega t - kx)} e^{-kz} e^{-\gamma t} \right\}$$

NOTE:

$$\frac{\gamma}{\omega} \sim h^2 \left( \frac{2\nu}{\sqrt{hg}} \right)$$

$\delta^2 = \text{BOUNDARY LAYER}$

How Big?

$$h = \frac{2\pi}{\lambda} \quad D = 10 \text{ cm} = 0.1 \text{ m} \quad \nu = 10^{-6} \frac{\text{m}^2}{\text{sec}}$$

$$\omega = \frac{2\pi}{T} \quad T \sim \frac{1}{4} \text{ sec} \quad \omega = \sqrt{hg}$$

$$\frac{2\nu}{\omega} \sim \frac{2 \cdot 10^{-6}}{8\pi} \sim 10^{-7} \text{ m}^2 \quad h^2 \left( \frac{2\nu}{\sqrt{hg}} \right) \sim 10^{-3} \ll 1$$